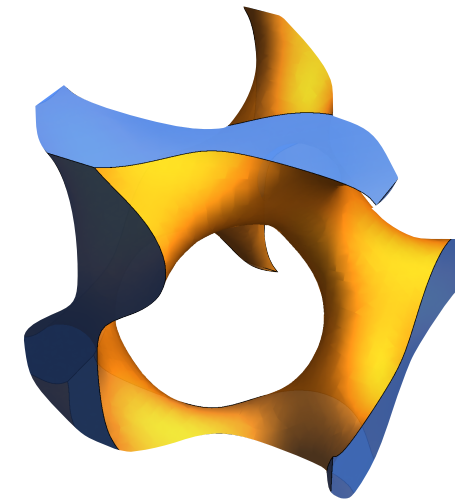
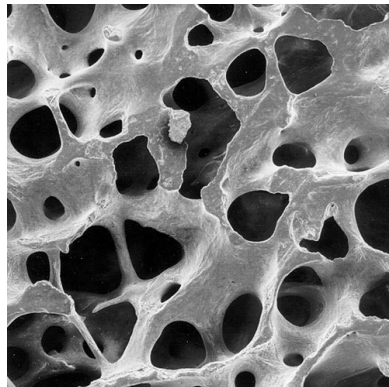
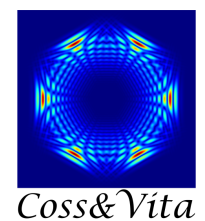


Generalised continua in biomechanics : from multi scale tissues to biomechanical metamaterials



Giuseppe Rosi, Nicolas Auffray

Multi-Scale Modelling and Simulation Laboratory
Laboratoire Modélisation et Simulation Multi-Echelle
Université Paris-Est CNRS UMR 8208



ELADYN-BIO workshop
12-11-2020



Financed by: IRP Coss&Vita and ANR MAX-OASIS

Context : elastic waves and ultrasounds

Elastic waves are currently used in several fields, such as non-destructive evaluation, characterisation, and diagnostics.

Principle : when a wave propagates inside a material, it carries information about the mechanical properties of the material itself.

Information is extracted solving an **inverse problem**.

Context : elastic waves and ultrasounds

Elastic waves are currently used in several fields, such as non-destructive evaluation, characterisation, and diagnostics.

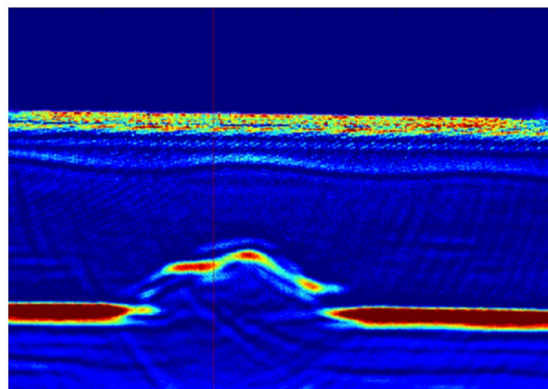
Principle : when a wave propagates inside a material, it carries information about the mechanical properties of the material itself.

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Main strategies:

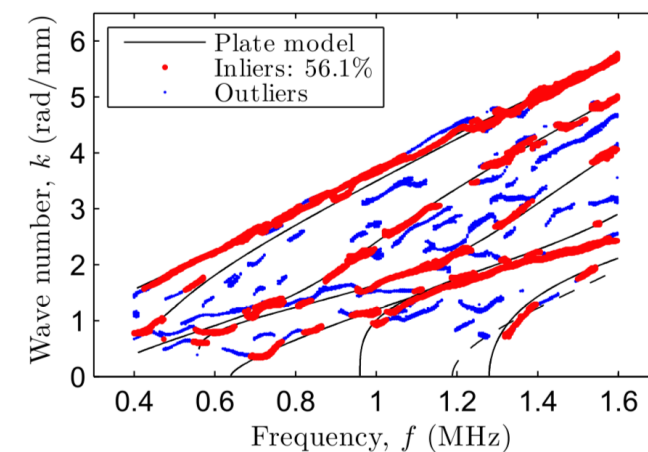
Time of flight, amplitude

Bulk propagation and reflections at boundaries (imaging)



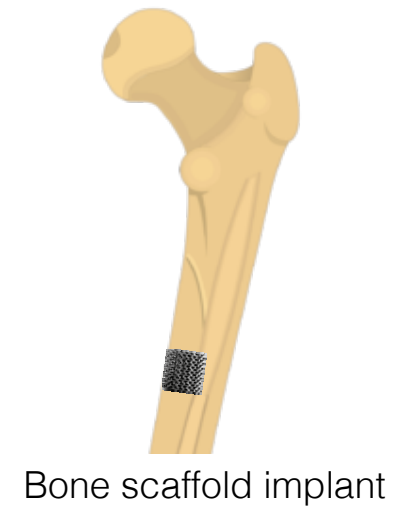
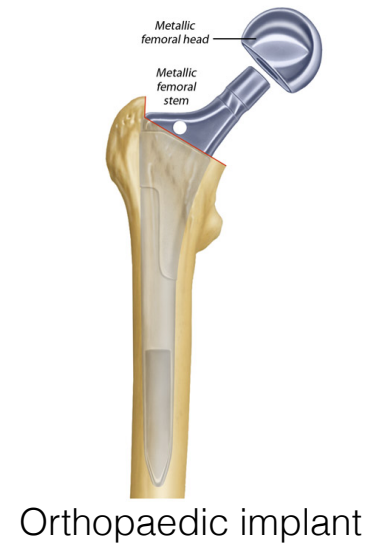
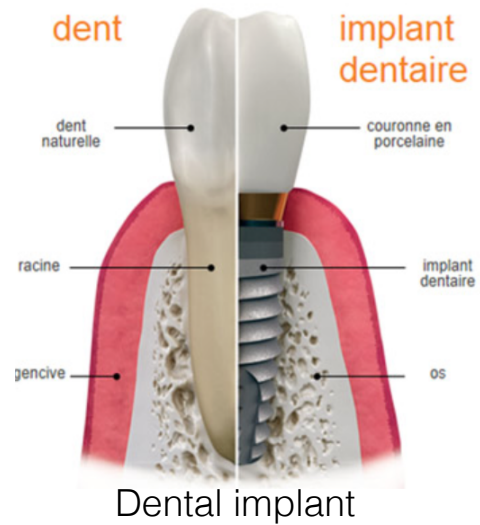
Dispersion

Guided propagation (surface waves, Lamb waves)



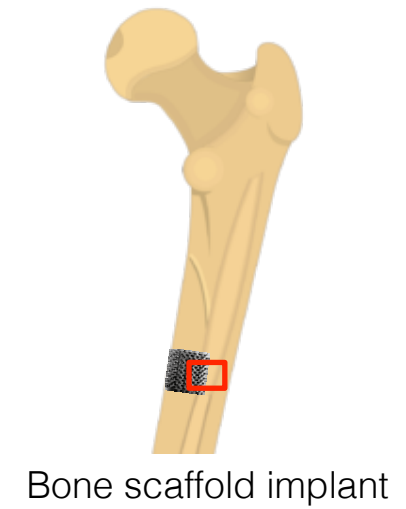
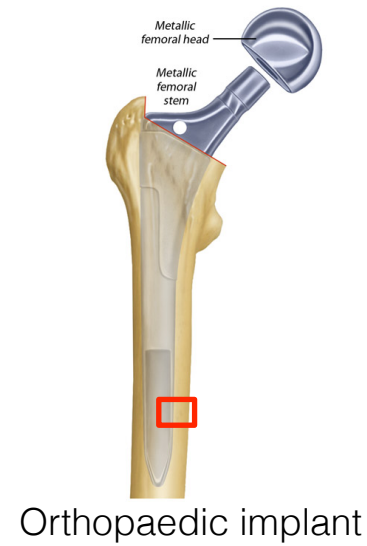
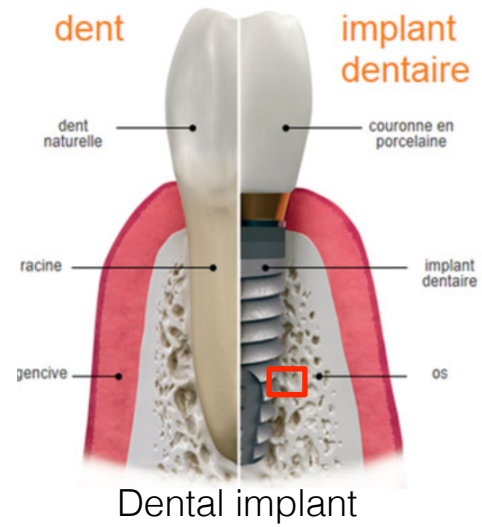
Multi scale tissue modelling and characterisation

Organ scale

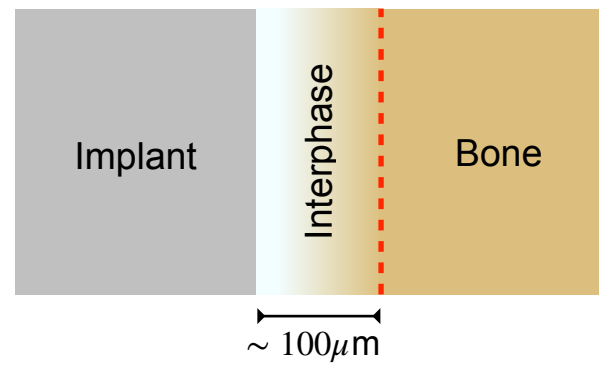


Multi scale tissue modelling and characterisation

Organ scale

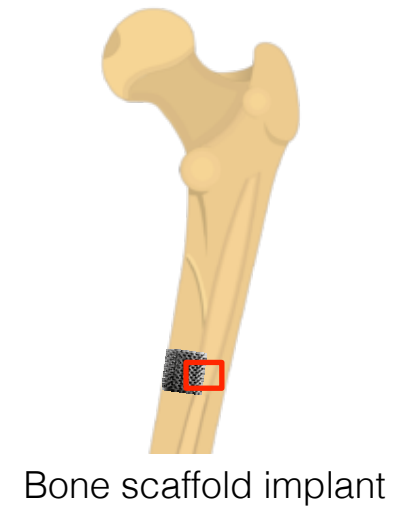
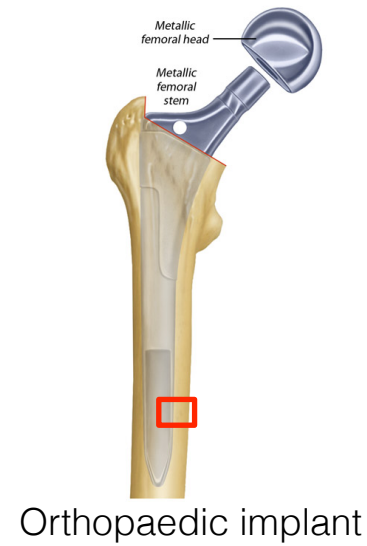
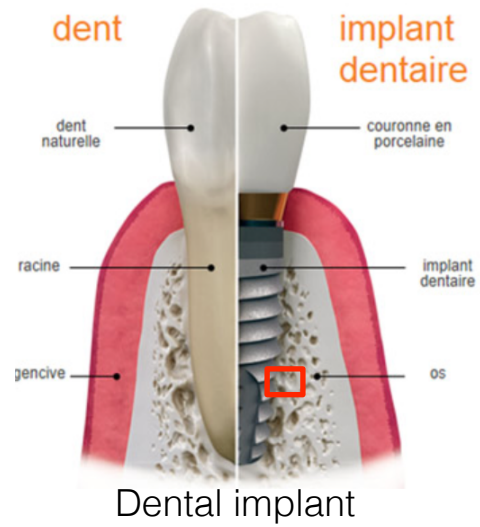


Tissue scale

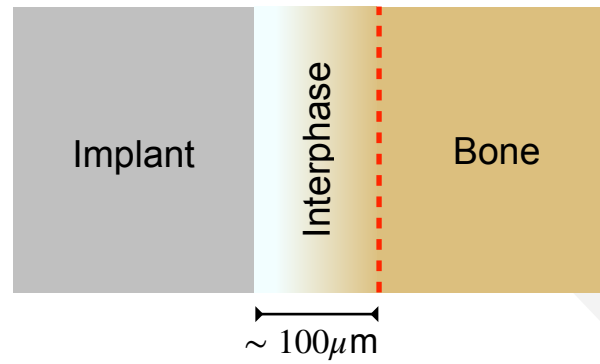


Multi scale tissue modelling and characterisation

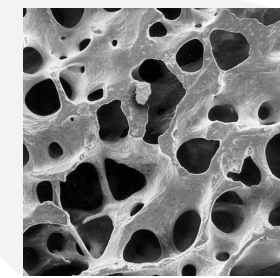
Organ scale



Tissue scale



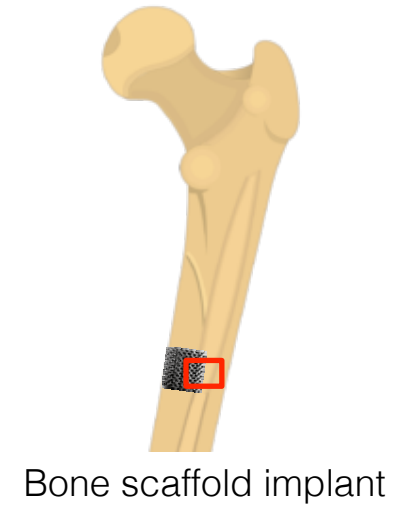
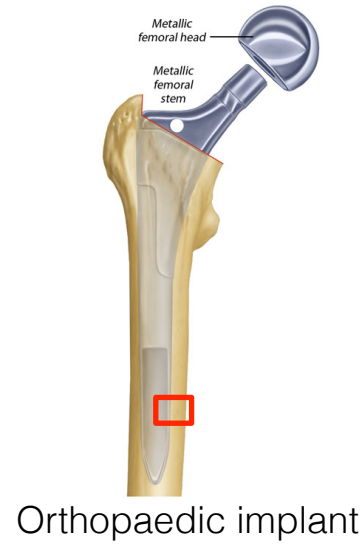
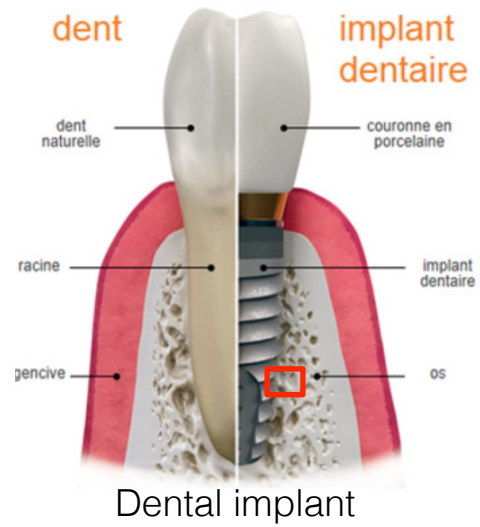
Architecture scale



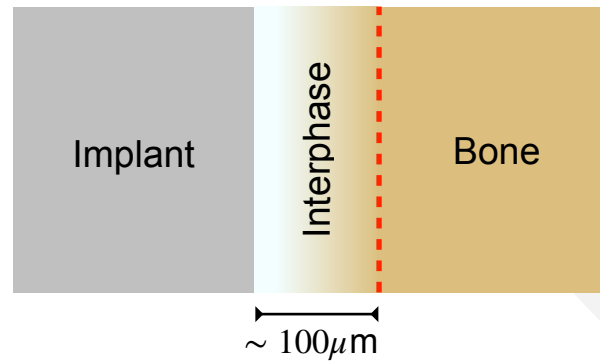
Bone

Multi scale tissue modelling and characterisation

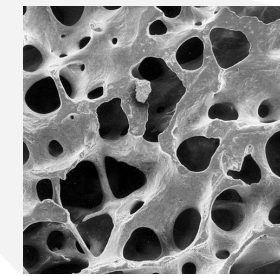
Organ scale



Tissue scale



Architecture scale



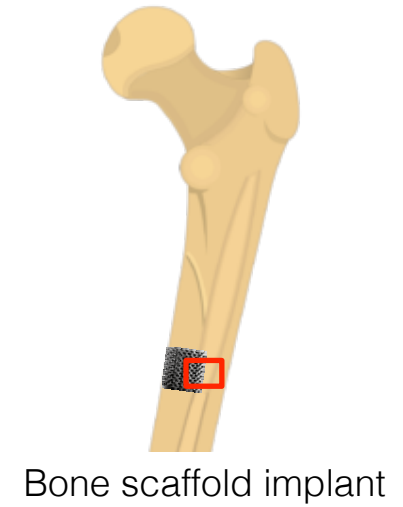
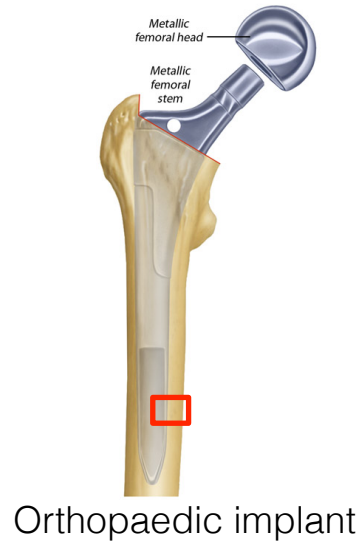
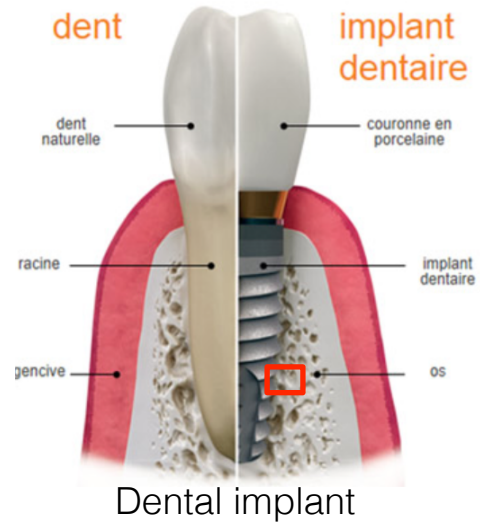
Bone

Modelling challenges

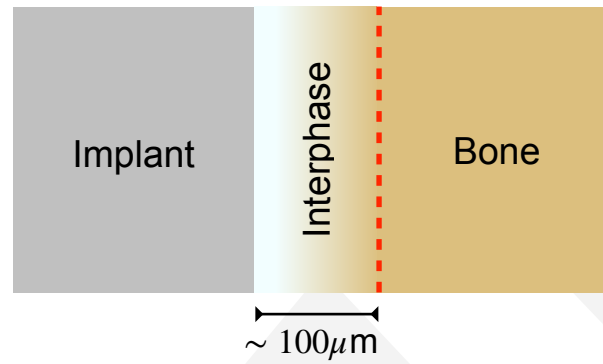
- Multi-scale architecture
- Heterogeneity
- Porosity
- Remodelling
- Boundary conditions

Multi scale tissue modelling and characterisation

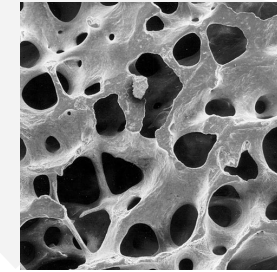
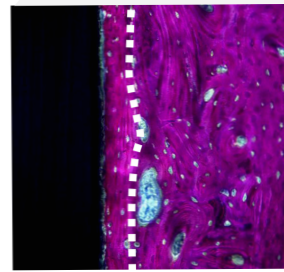
Organ scale



Tissue scale



Architecture scale



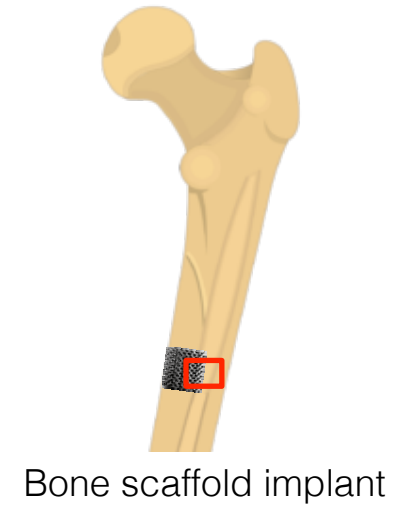
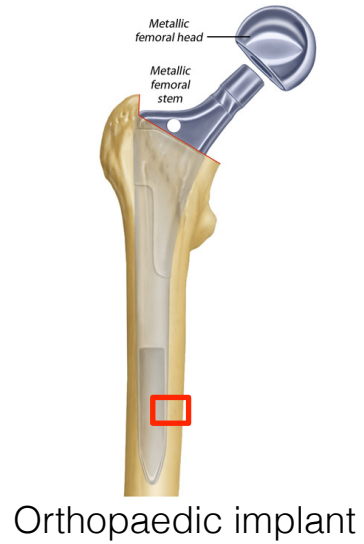
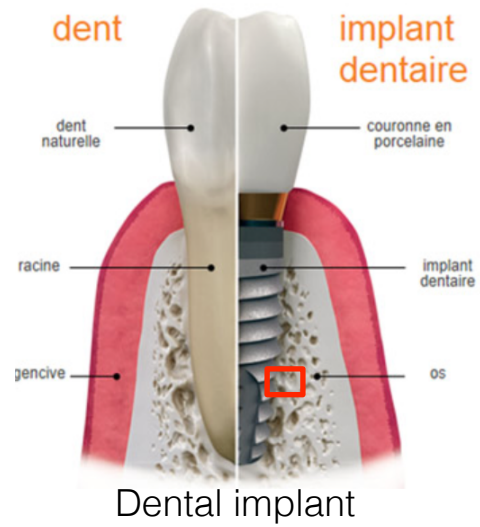
Modelling challenges

Heterogeneity
Mesh refinement
Computational costs
Evolving conditions (osteointegration)
Boundary conditions

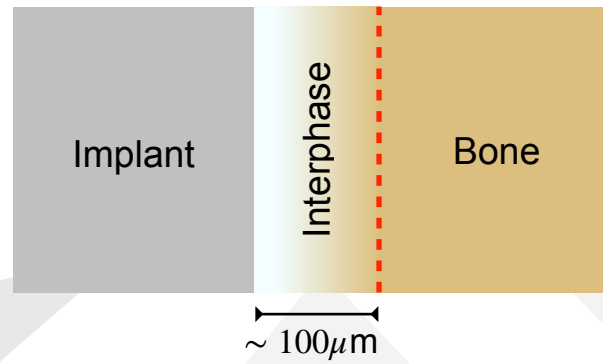
Multi-scale architecture
Heterogeneity
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Multi scale tissue modelling and characterisation

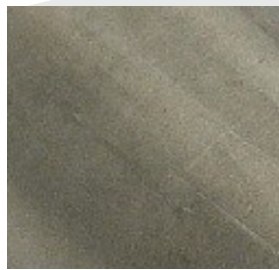
Organ scale



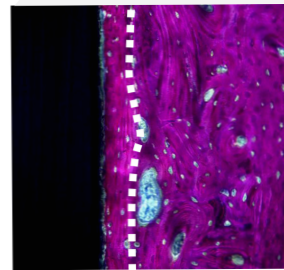
Tissue scale



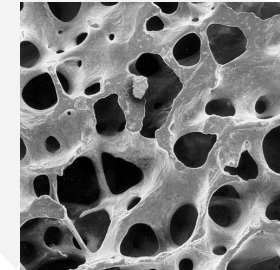
Architecture scale



Implant



Interphase



Bone

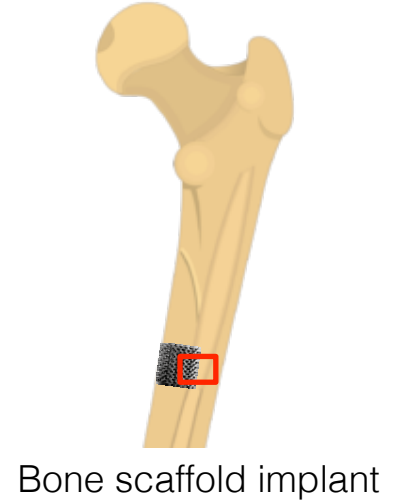
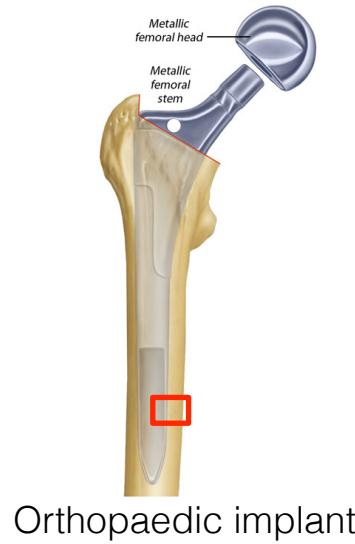
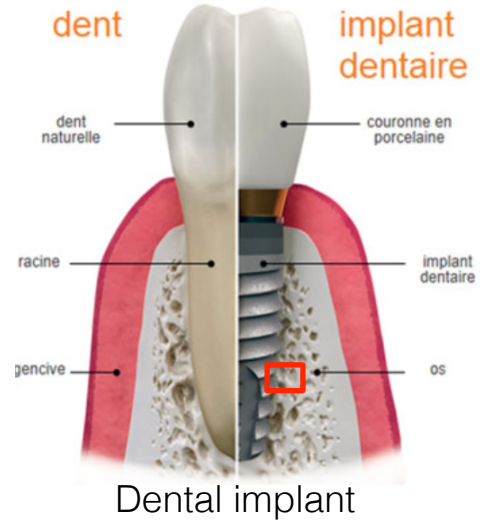
Modelling challenges

- Heterogeneity
- Mesh refinement
- Computational costs
- Evolving conditions (osteointegration)
- Boundary conditions

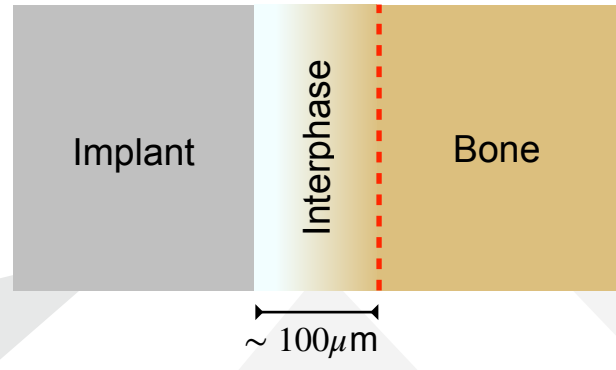
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- Remodelling
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Multi scale tissue modelling and characterisation

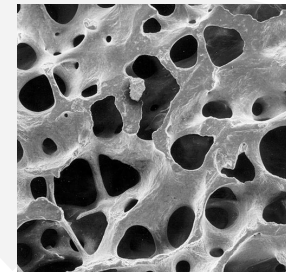
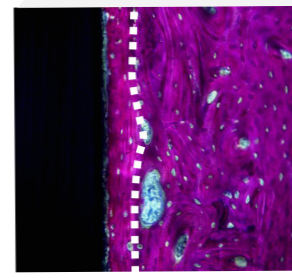
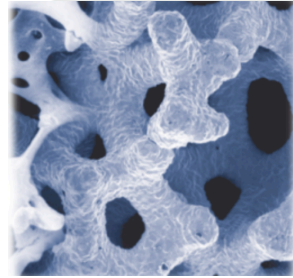
Organ scale



Tissue scale



Architecture scale



Modelling challenges

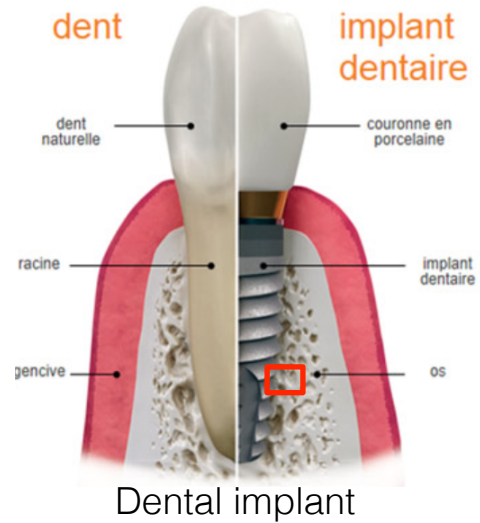
- Multi-scale architecture
- Porosity
- Tissue engineering
- Multiple optimisation constraints
- Boundary conditions

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- Boundary conditions

- Multi-scale architecture
- Heterogeneity
- Porosity
- Remodelling
- Boundary conditions

Multi scale tissue modelling and characterisation

Organ scale



Dental implant

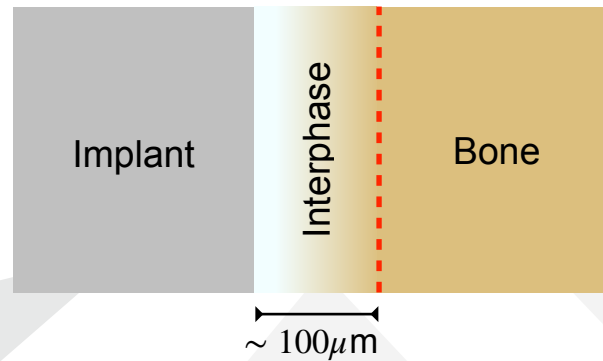


Orthopaedic implant

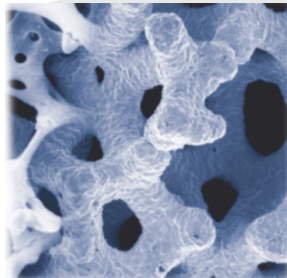


Bone scaffold implant

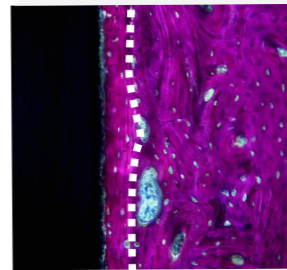
Tissue scale



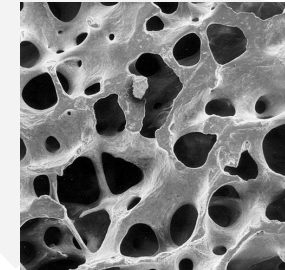
Architecture scale



Implant



Interphase



Bone

Modelling challenges

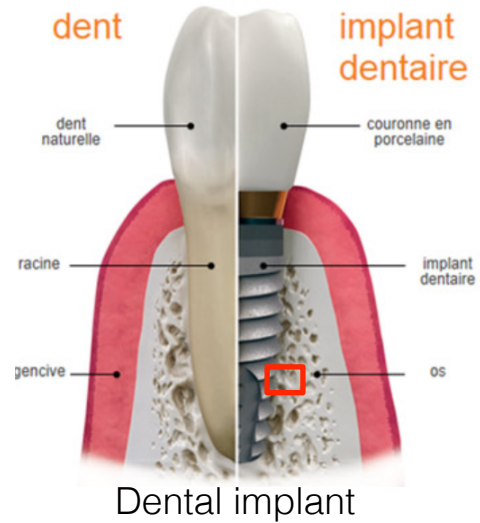
- Multi-scale architecture
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Multi scale tissue modelling and characterisation

Organ scale



Dental implant

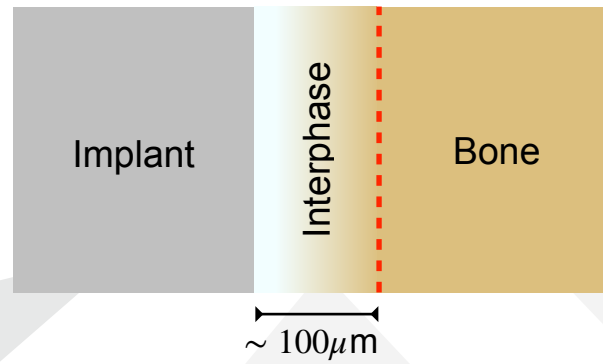


Orthopaedic implant

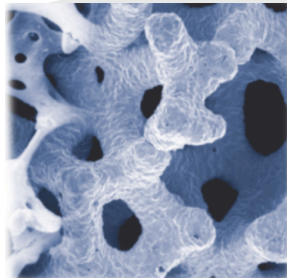


Bone scaffold implant

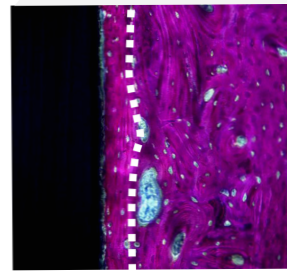
Tissue scale



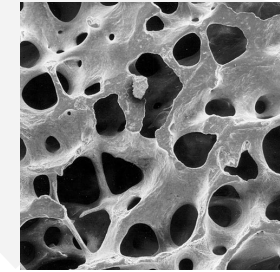
Architecture scale



Implant



Interphase



Bone

Modelling challenges

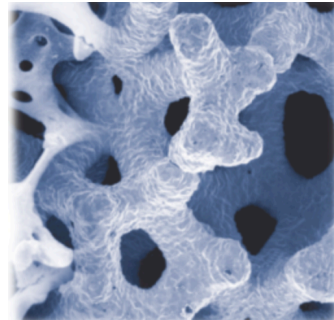
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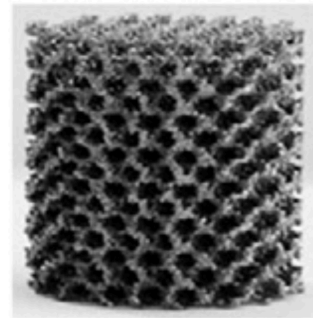
- Multi-scale architecture
- Heterogeneity
- Porosity
- Remodelling
- Boundary conditions

Architected implants as biomechanical metamaterials

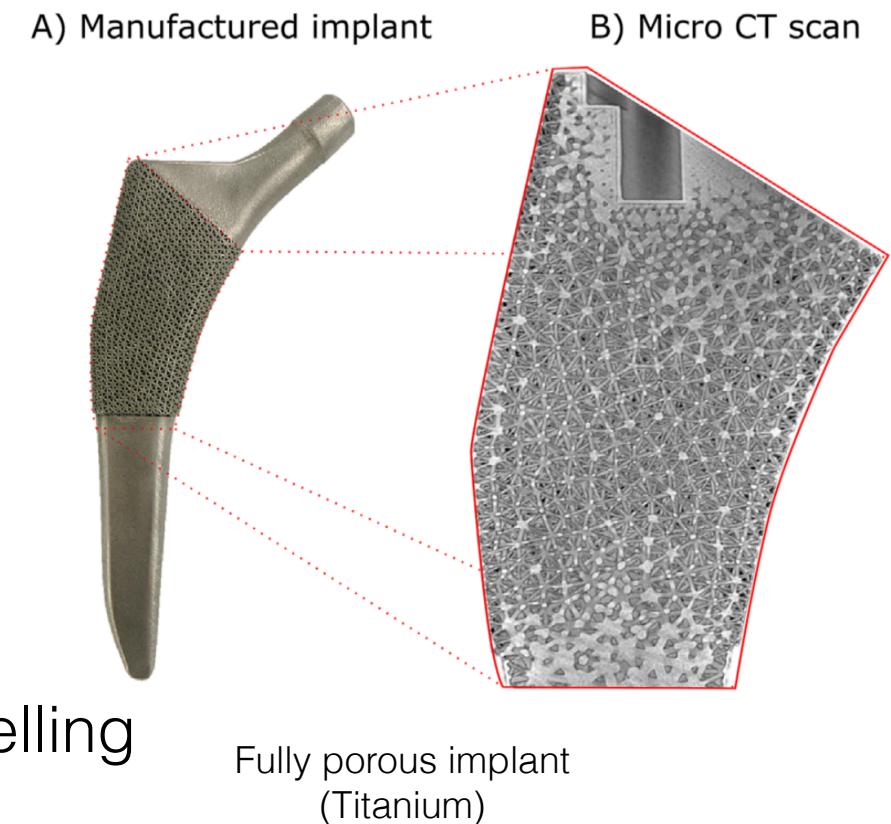
Optimisation of the mechanical properties or reduction of stress shielding



Zimmer's
Trabecular metal™
(Tantalum)



Gyroid scaffold
(Titanium)



Challenges and objectives:

- Take into account architecture and size effects in modelling
- Enhanced monitoring of the state of the implant
- Cost (or utility) functions to be used in optimisation

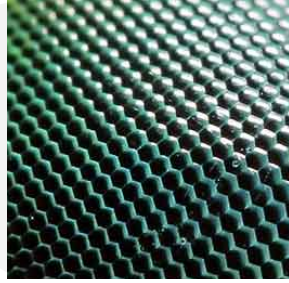
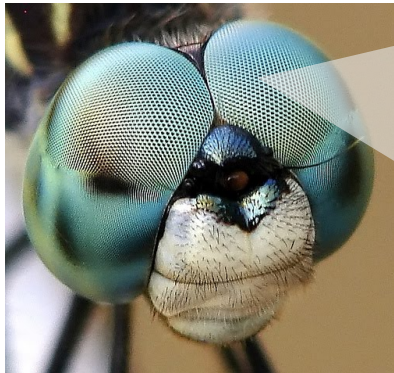
Results developed for metamaterials can be used

Yáñez, A. et al. (2018). Gyroid porous titanium structures: A versatile solution to be used as scaffolds in bone defect reconstruction. *Materials & Design*, 140, 21–29.

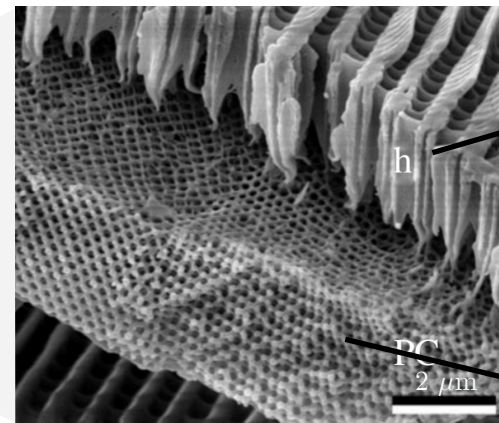
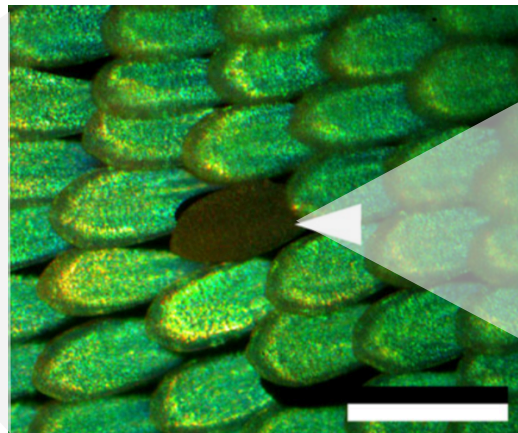
Arabnejad, S. et al. (2017). Fully porous 3D printed titanium femoral stem to reduce stress-shielding following total hip arthroplasty. *Journal of Orthopaedic Research*, 35(8), 1774–1783.

Nature loves regular architectures!

Hexagonal honeycomb maximise the area vs the perimeter (for regular tilings) and isotropic mechanical properties



Gyroids are a minimal surfaces (obtained e.g. as assembly of co-block polymers) and are used as photonic crystals



Honeycomb

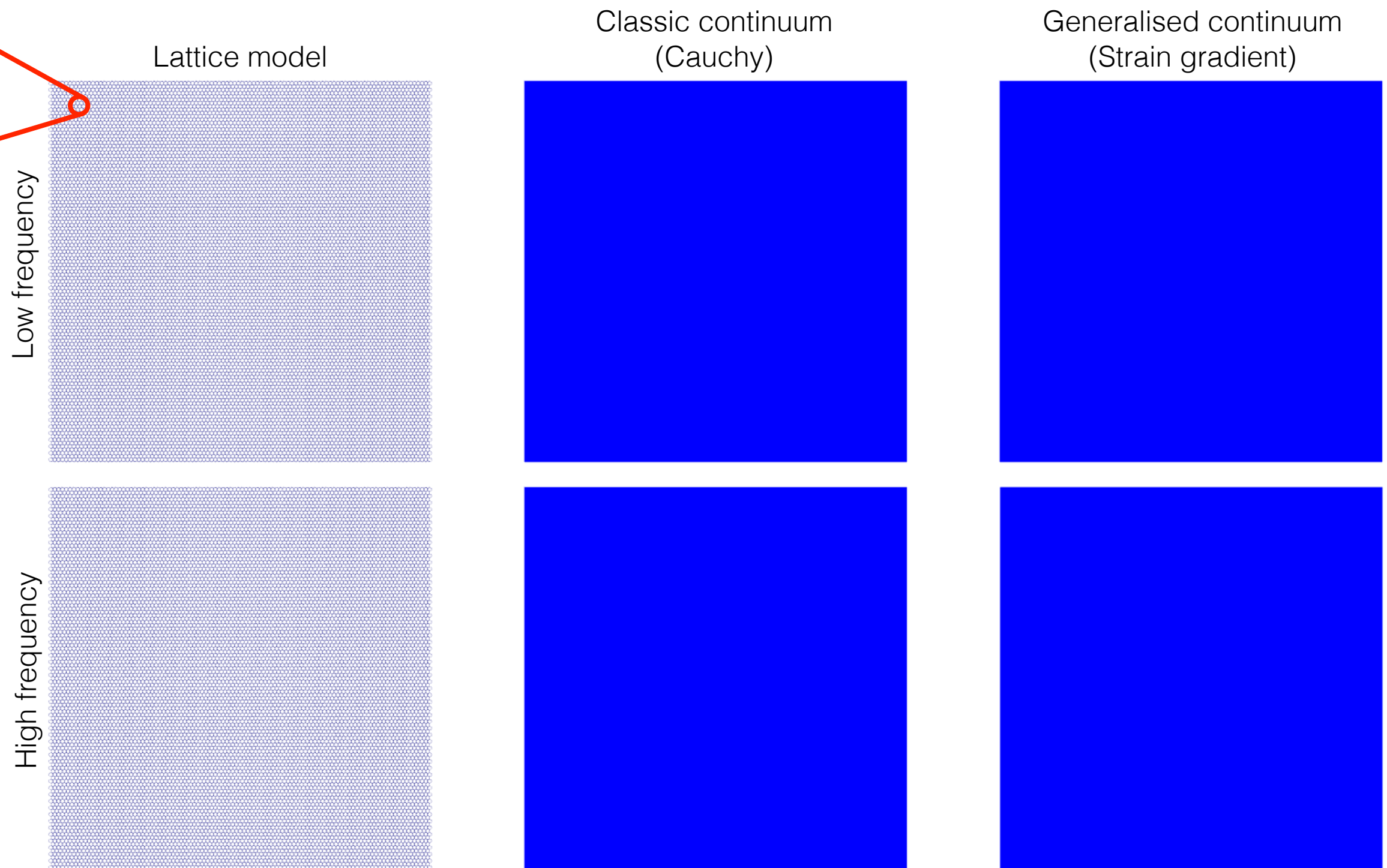
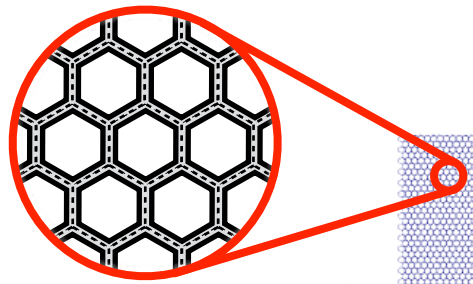
Gyroid

Hales, T. C. (2001). The Honeycomb Conjecture. *Discrete & Computational Geometry*, 25(1), 1–22.

Dolan et al. (2014). Optical Properties of Gyroid Structured Materials: From Photonic Crystals to Metamaterials. *Advanced Optical Materials*, 3(1), 12–32.

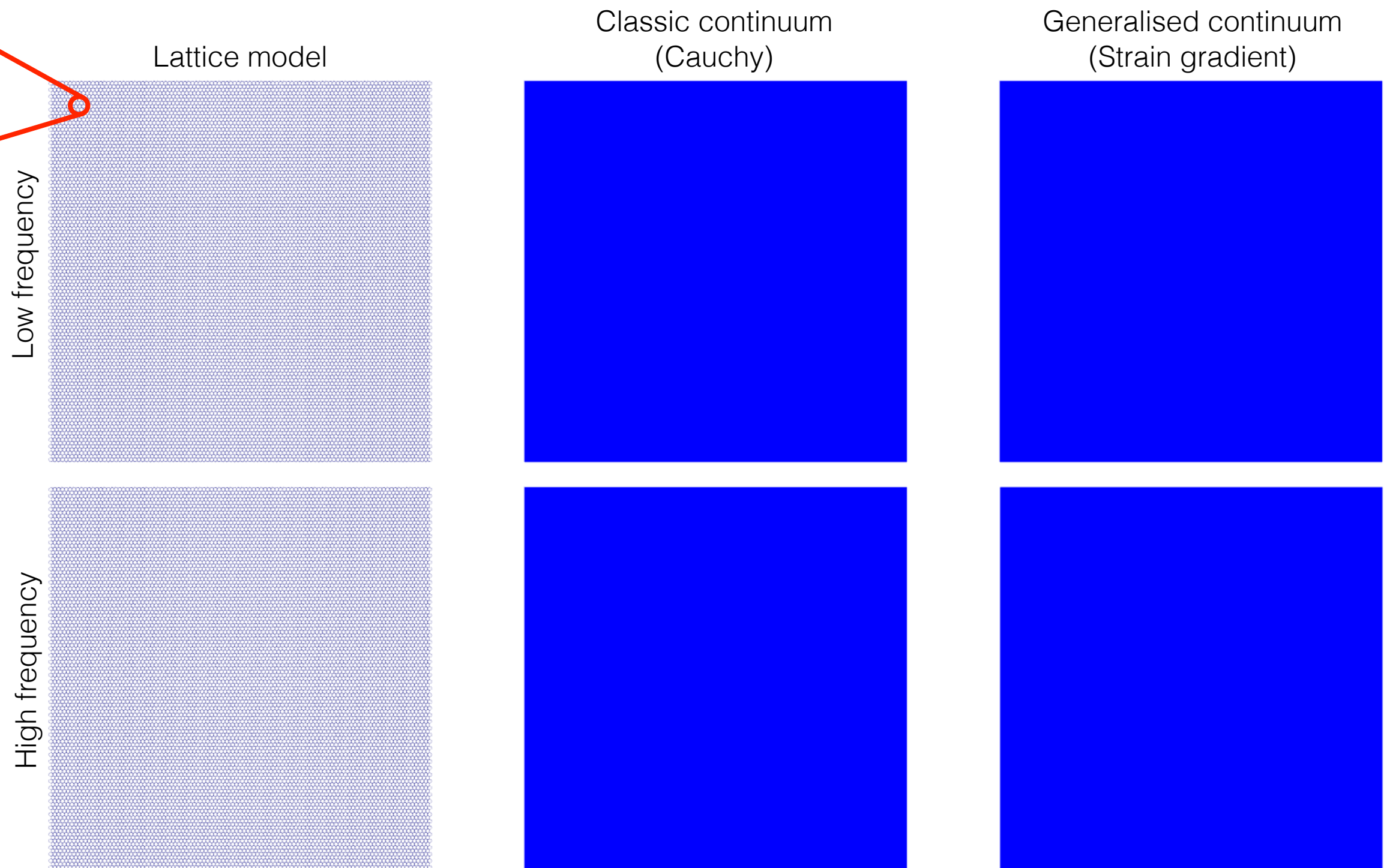
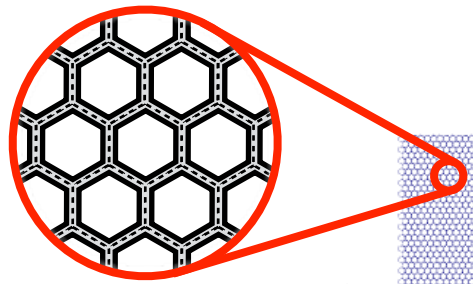
Wilts, B. D. et al (2012) Iridescence and spectral filtering of the gyroid-type photonic crystals in *Parides sesostris* wing scales. *Interface Focus*.

Wave propagation in hexagonal honeycombs



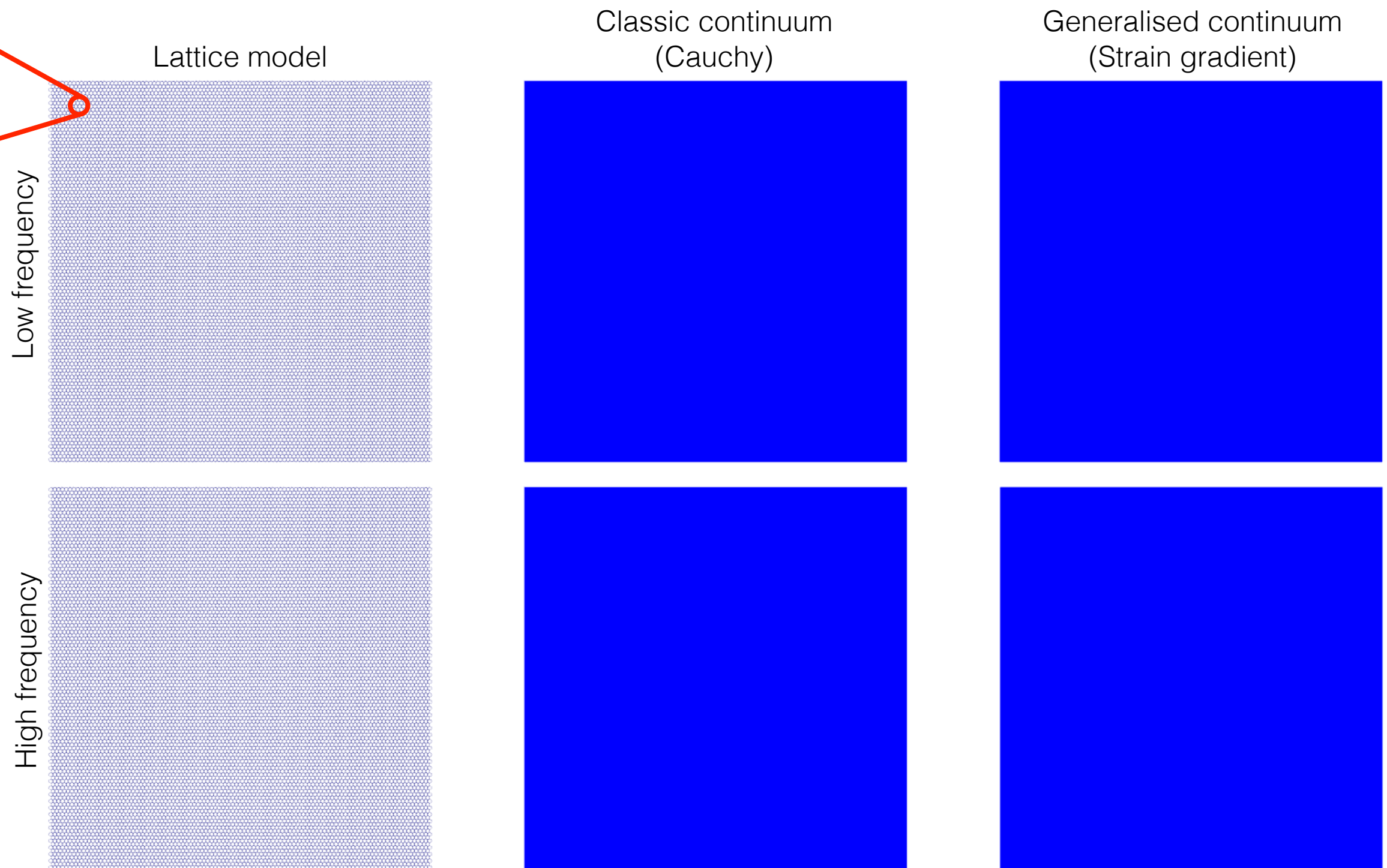
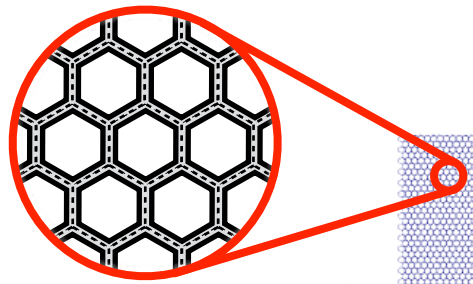
Wave propagation in architected materials is not fully captured by a classic continuum

Wave propagation in hexagonal honeycombs



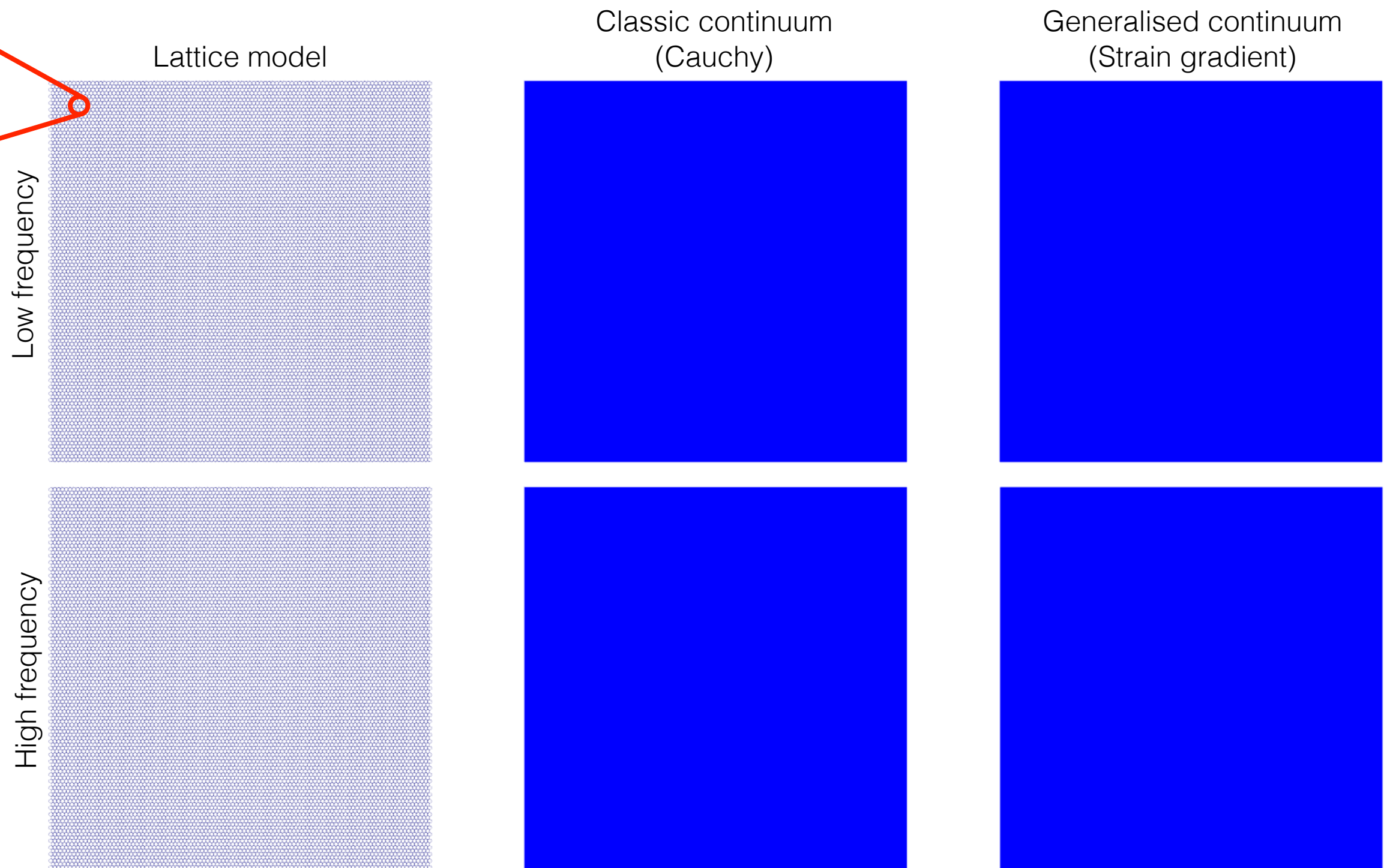
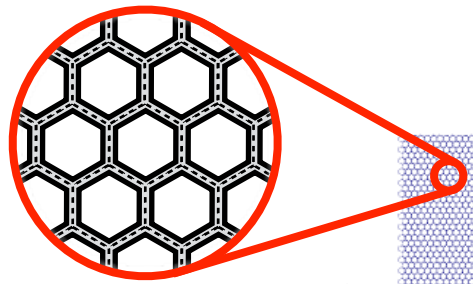
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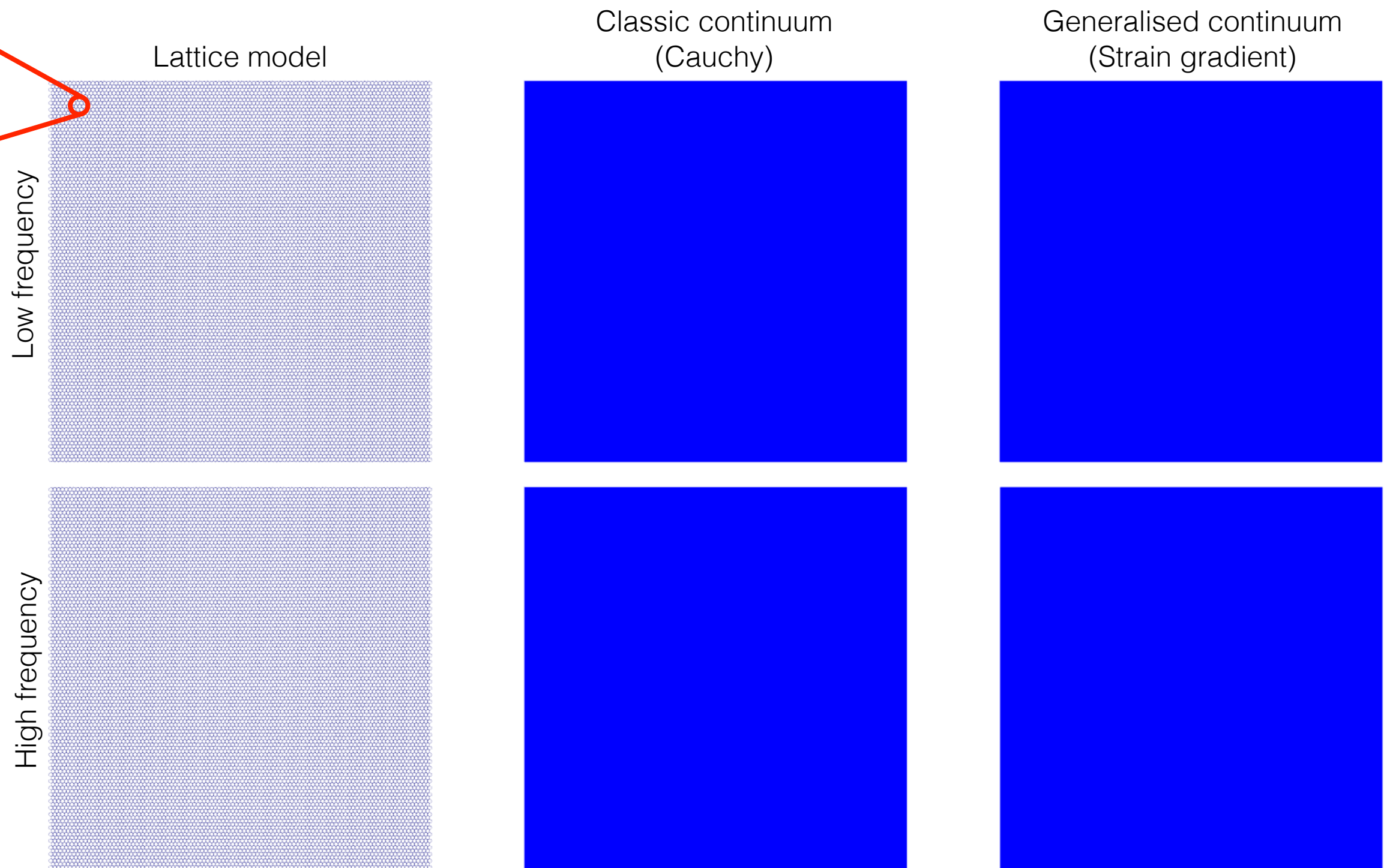
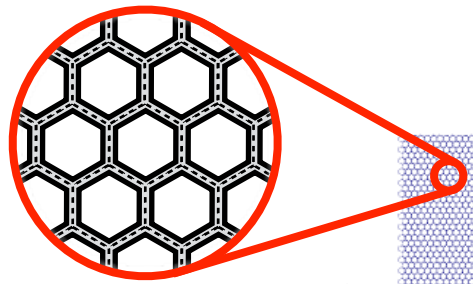
Wave propagation in architected materials is not fully captured by a classic continuum

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Wave propagation in architected materials is not fully captured by a classic continuum

Wave propagation in hexagonal honeycombs



Wave propagation in architected materials is not fully captured by a classic continuum

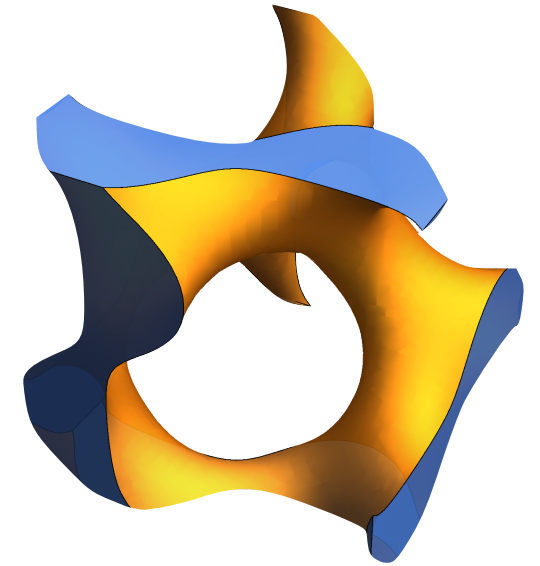
Wave propagation in gyroid lattices

Triply periodic minimal surface

Simple equation :

$$\sin(a\pi x)\cos(a\pi y) + \cos(a\pi x)\sin(a\pi z) + \sin(a\pi y)\cos(a\pi z) = b$$

Two parameters a, b to control cell size and the porosity



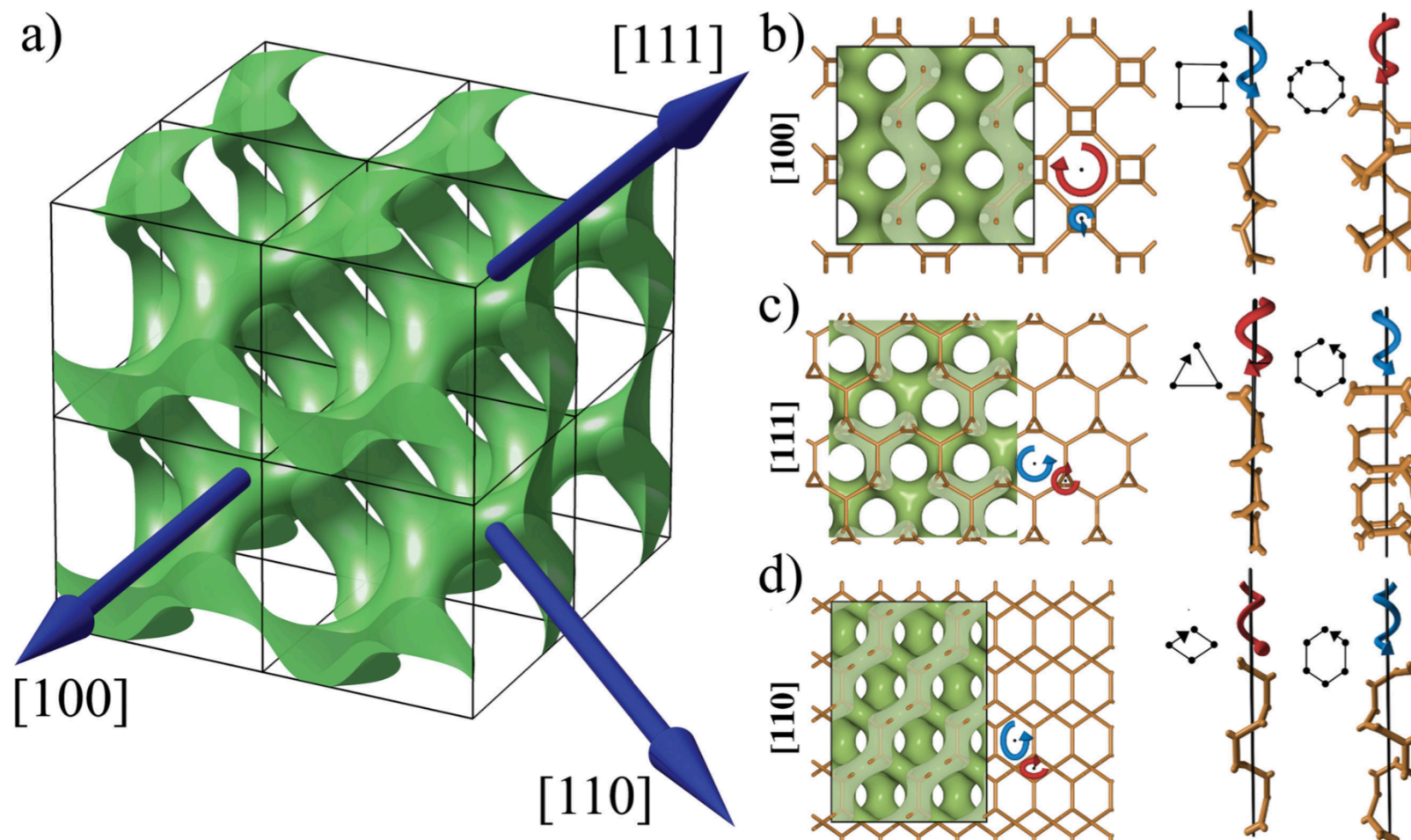
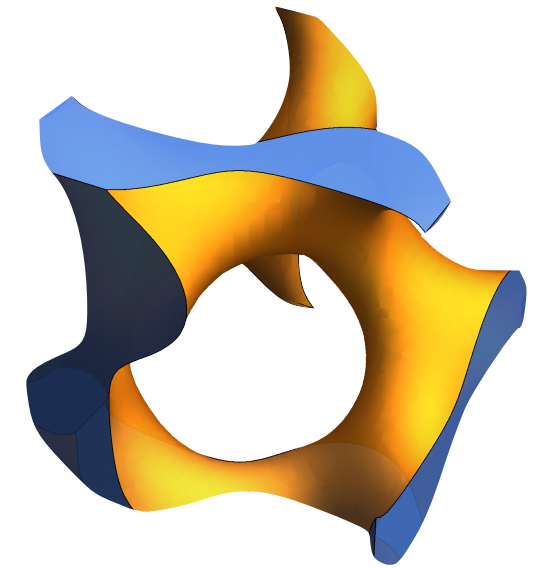
Wave propagation in gyroid lattices

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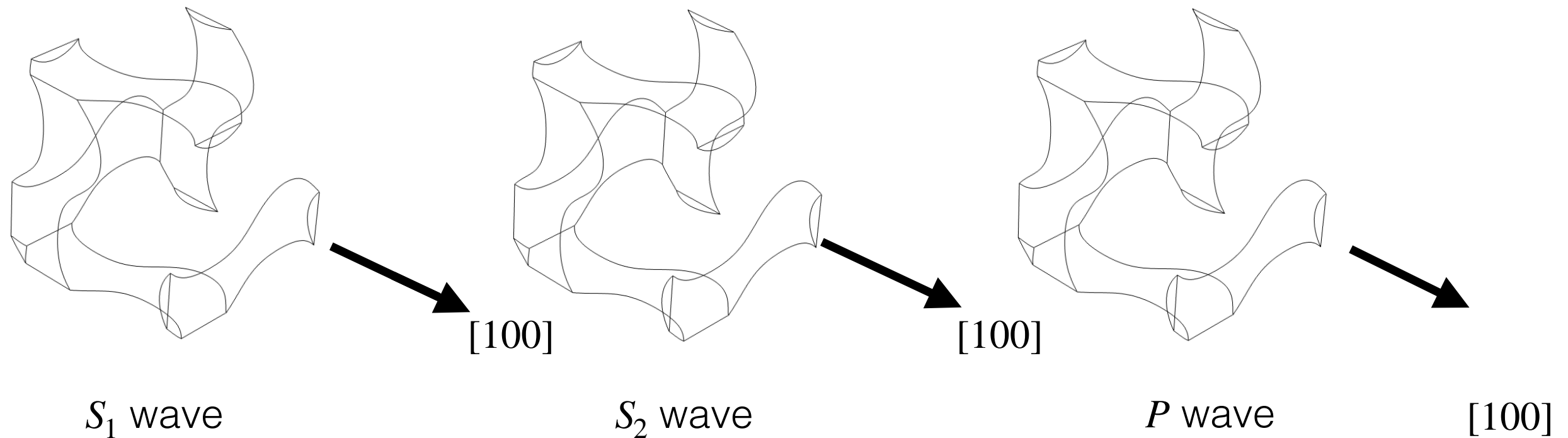
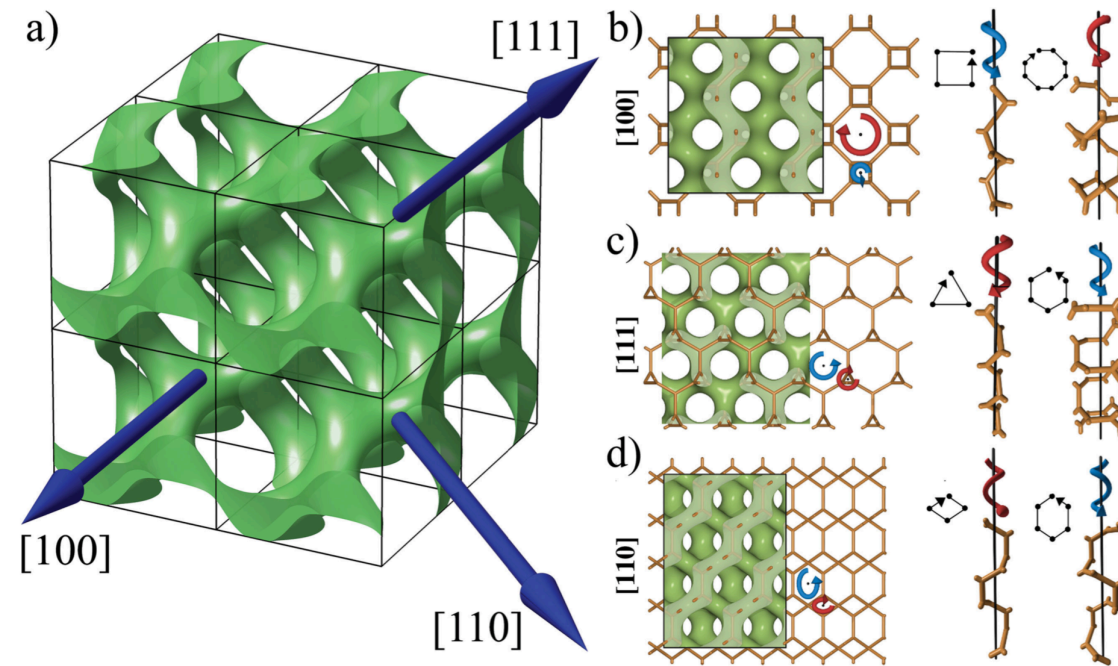
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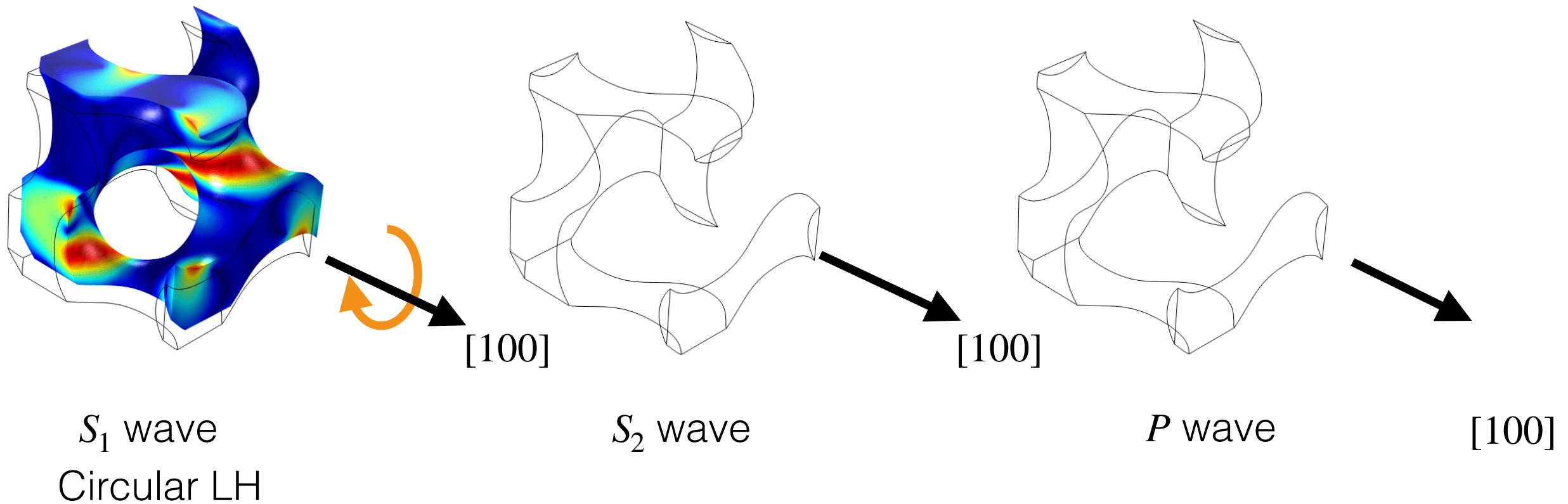
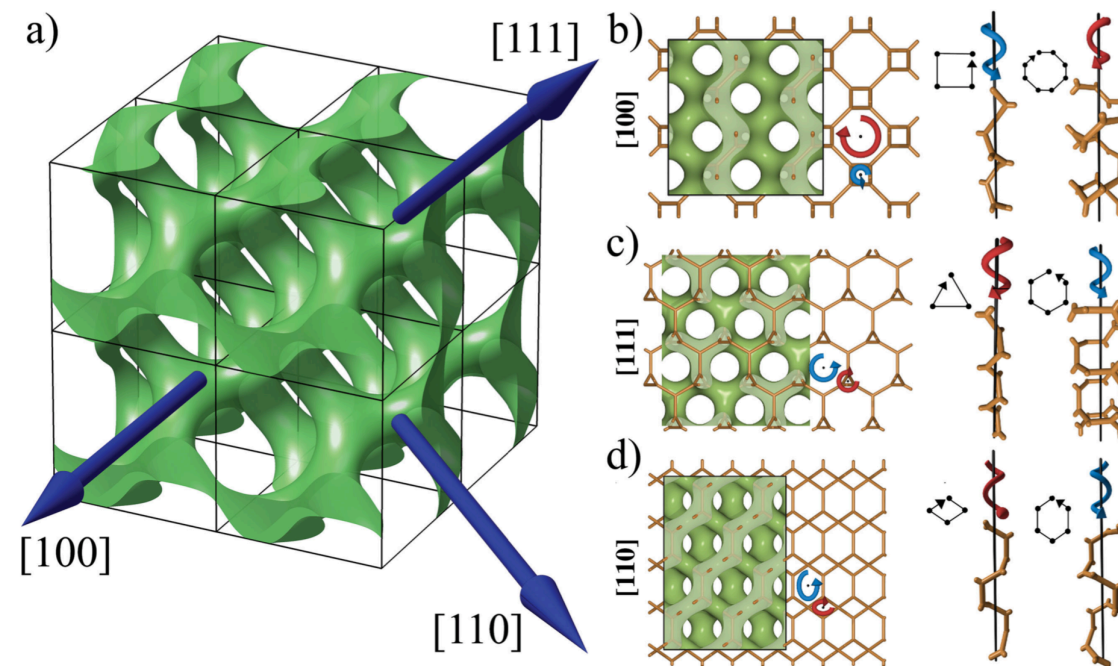
Two parameters a, b to control cell size and the porosity



Wave propagation in gyroid lattices



Wave propagation in gyroid lattices



S_1 wave

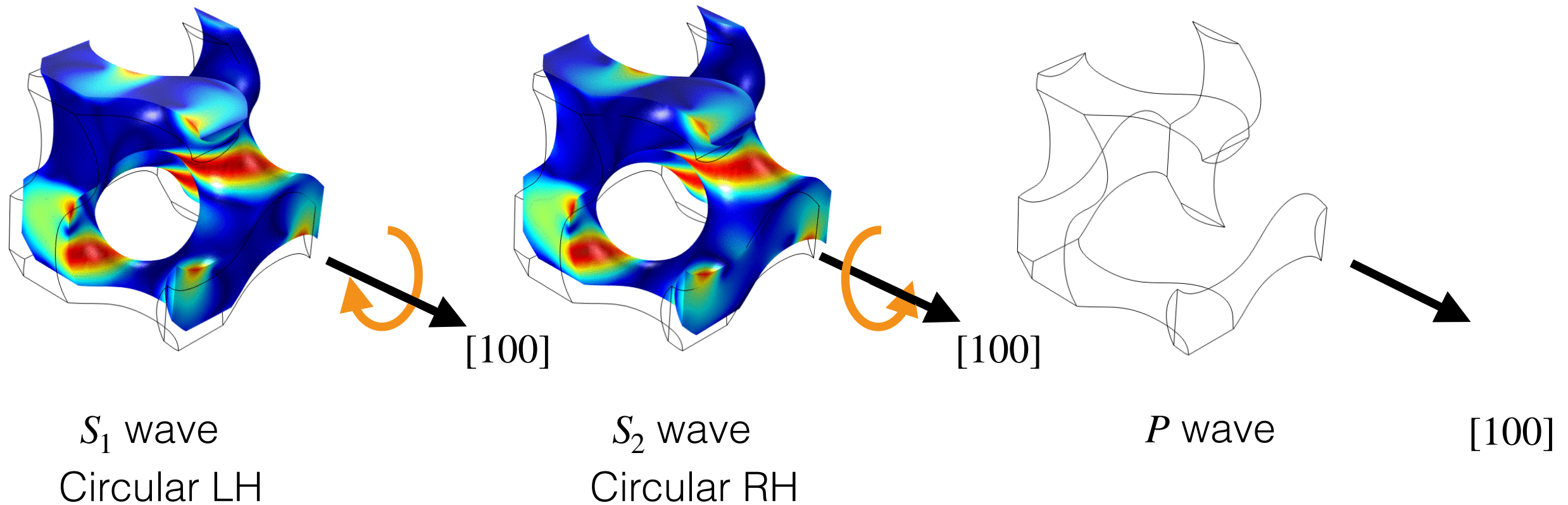
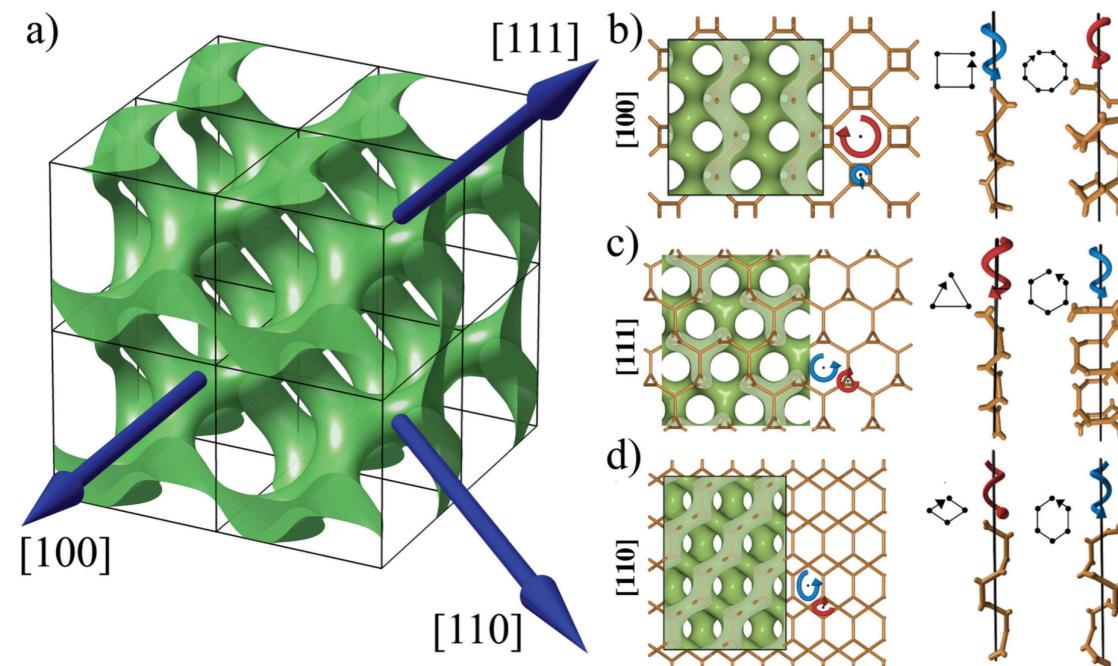
Circular LH

S_2 wave

P wave

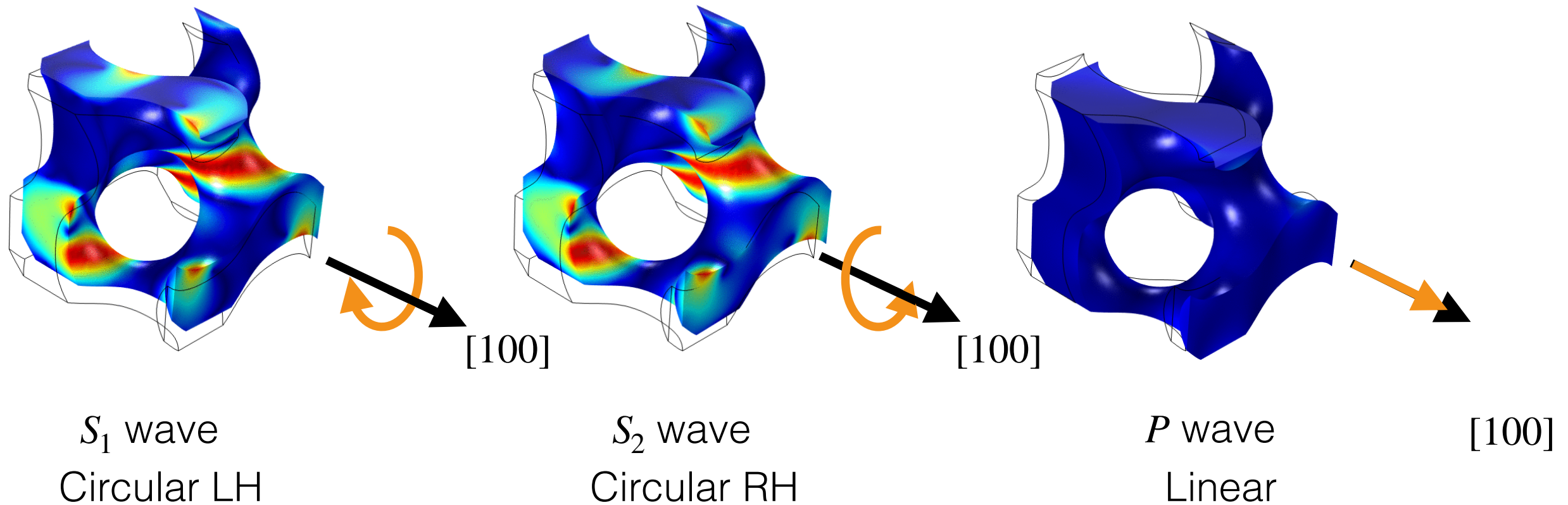
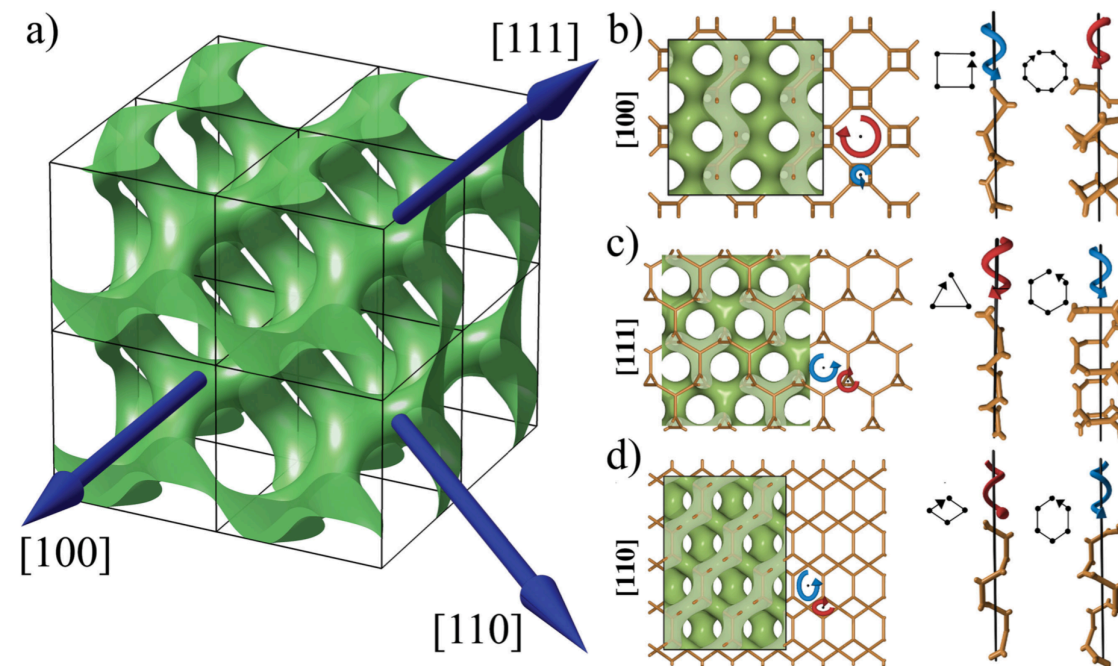
[100]

Wave propagation in gyroid lattices



Rosi, G., Auffray, N., Combescure, C. (2020). On the failure of classic elasticity in predicting elastic wave propagation in gyroid lattices for very long wavelengths. Symmetry

Wave propagation in gyroid lattices



Rosi, G., Auffray, N., Combescure, C. (2020). On the failure of classic elasticity in predicting elastic wave propagation in gyroid lattices for very long wavelengths. Symmetry

Overview of the strain gradient model

Elastic energy

$$\frac{1}{2} (\underline{\underline{\sigma}} : \underline{\underline{\varepsilon}})$$

Strain tensor

Stress tensor

Kinetic energy

$$\frac{1}{2} (\underline{\underline{p}} \cdot \underline{\dot{\underline{u}}})$$

Velocity

Momentum

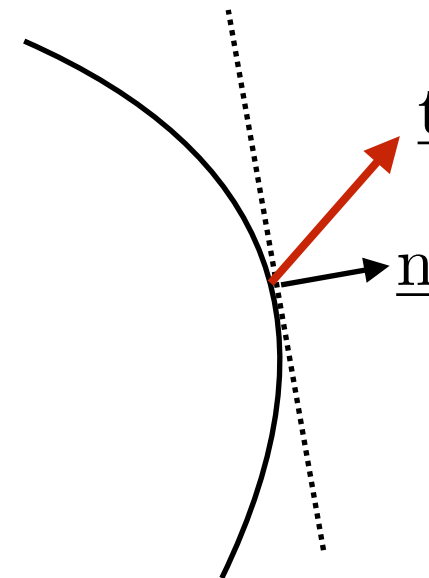
Balance equation

$$\nabla \cdot (\underline{\underline{\sigma}}) = \underline{\dot{\underline{p}}}$$

Boundary conditions

Traction

$$\underline{\underline{t}} = (\underline{\underline{\sigma}}) \underline{\underline{n}}$$



Overview of the strain gradient model

Elastic energy

$$\frac{1}{2} \left(\underline{\underline{\sigma}} : \underline{\underline{\varepsilon}} \right) + \frac{1}{2} \left(\underline{\underline{\tau}} : \nabla \underline{\underline{\varepsilon}} \right)$$

Strain tensor $\underline{\underline{\varepsilon}}$ Gradient of strain tensor $\nabla \underline{\underline{\varepsilon}}$
 Stress tensor $\underline{\underline{\sigma}}$ Hyper-Stress tensor $\underline{\underline{\tau}}$

Kinetic energy

$$\frac{1}{2} \left(\underline{\underline{p}} \cdot \dot{\underline{\underline{u}}} \right)$$

Velocity $\dot{\underline{\underline{u}}}$
 Momentum $\underline{\underline{p}}$

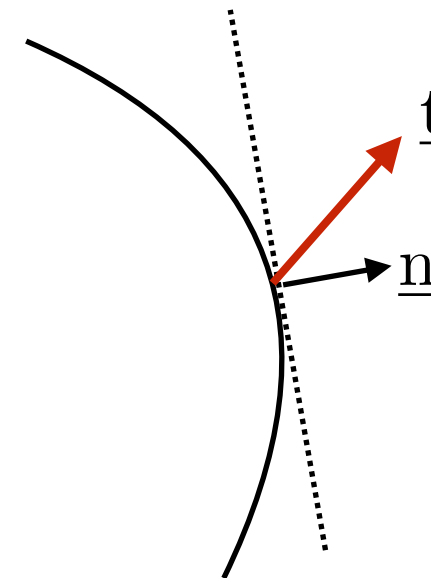
Balance equation

$$\nabla \cdot \left(\underline{\underline{\sigma}} \right) = \dot{\underline{\underline{p}}}$$

Boundary conditions

Traction

$$\underline{\underline{t}} = \left(\underline{\underline{\sigma}} \right) \underline{\underline{n}}$$



Overview of the strain gradient model

Elastic energy

$$\frac{1}{2} \left(\underset{\sim}{\sigma} : \underset{\sim}{\varepsilon} \right) + \frac{1}{2} \left(\underset{\sim}{\tau} : \nabla \underset{\sim}{\varepsilon} \right)$$

Labels for the Elastic energy equation:
 - Stress tensor: $\underset{\sim}{\sigma}$
 - Strain tensor: $\underset{\sim}{\varepsilon}$
 - Hyper-Stress tensor: $\underset{\sim}{\tau}$
 - Gradient of strain tensor: $\nabla \underset{\sim}{\varepsilon}$

Kinetic energy

$$\frac{1}{2} \left(\underline{\underline{p}} \cdot \underline{\underline{\dot{u}}} \right) + \frac{1}{2} \left(\underset{\sim}{q} : \nabla \underline{\underline{\dot{u}}} \right)$$

Labels for the Kinetic energy equation:
 - Momentum: $\underline{\underline{p}}$
 - Velocity: $\underline{\underline{\dot{u}}}$
 - Hyper momentum: $\underset{\sim}{q}$
 - Gradient of velocity: $\nabla \underline{\underline{\dot{u}}}$

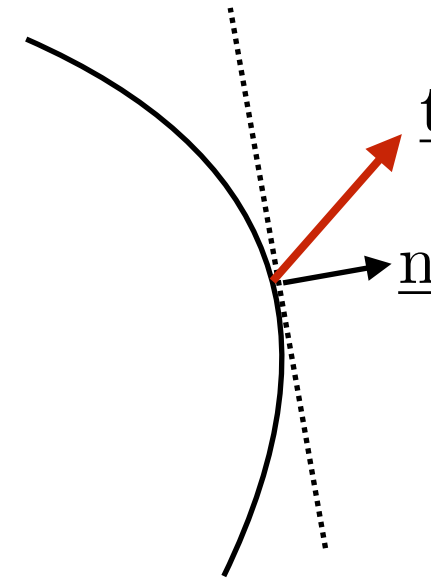
Balance equation

$$\nabla \cdot \left(\underset{\sim}{\sigma} \right) = \underline{\underline{\dot{p}}}$$

Boundary conditions

Traction

$$\underline{\underline{t}} = \left(\underset{\sim}{\sigma} \right) \underline{\underline{n}}$$



Overview of the strain gradient model

Elastic energy

$$\frac{1}{2} \left(\underset{\text{Stress tensor}}{\underline{\underline{\sigma}}} : \underset{\text{Strain tensor}}{\underline{\underline{\varepsilon}}} \right) + \frac{1}{2} \left(\underset{\text{Hyper-Stress tensor}}{\underline{\underline{\tau}}} : \underset{\text{Gradient of strain tensor}}{\nabla \underline{\underline{\varepsilon}}} \right)$$

Kinetic energy

$$\frac{1}{2} \left(\underset{\text{Momentum}}{\underline{\underline{p}}} \cdot \underset{\text{Velocity}}{\dot{\underline{\underline{u}}}} \right) + \frac{1}{2} \left(\underset{\text{Hyper momentum}}{\underline{\underline{q}}} : \underset{\text{Gradient of velocity}}{\nabla \dot{\underline{\underline{u}}}} \right)$$

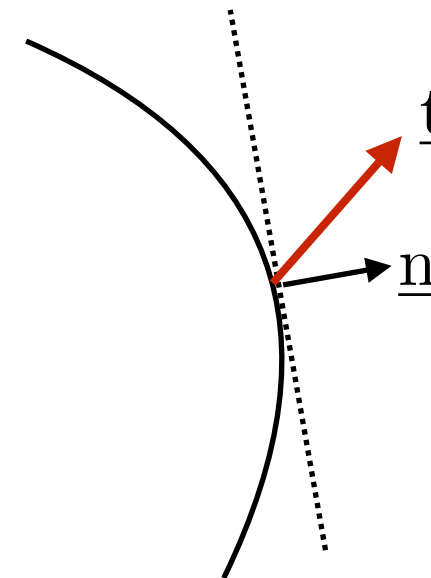
Balance equation

$$\nabla \cdot \left(\underline{\underline{\sigma}} - \nabla \cdot \underline{\underline{\tau}} \right) = \dot{\underline{\underline{p}}} - \nabla \cdot \dot{\underline{\underline{q}}}$$

Boundary conditions

Traction

$$\underline{\underline{t}} = \left(\underline{\underline{\sigma}} \quad \underline{\underline{\tau}} \right) \underline{\underline{n}}$$



Overview of the strain gradient model

Elastic energy

$$\frac{1}{2} \left(\underset{\sim}{\sigma} : \underset{\sim}{\varepsilon} \right) + \frac{1}{2} \left(\underset{\sim}{\tau} : \nabla \cdot \underset{\sim}{\varepsilon} \right)$$

Labels: Stress tensor ($\underset{\sim}{\sigma}$), Strain tensor ($\underset{\sim}{\varepsilon}$), Hyper-Stress tensor ($\underset{\sim}{\tau}$), Gradient of strain tensor ($\nabla \cdot \underset{\sim}{\varepsilon}$)

Kinetic energy

$$\frac{1}{2} \left(\underline{p} \cdot \underline{\dot{u}} \right) + \frac{1}{2} \left(\underset{\sim}{q} : \nabla \underline{\dot{u}} \right)$$

Labels: Momentum (\underline{p}), Velocity ($\underline{\dot{u}}$), Hyper momentum ($\underset{\sim}{q}$), Gradient of velocity ($\nabla \underline{\dot{u}}$)

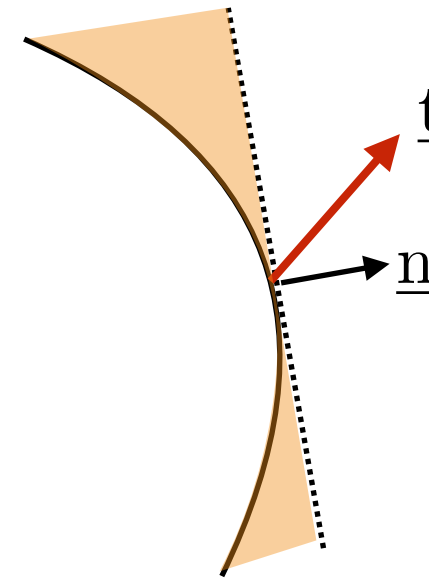
Balance equation

$$\nabla \cdot \left(\underset{\sim}{\sigma} - \nabla \cdot \underset{\sim}{\tau} \right) = \dot{\underline{p}} - \nabla \cdot \dot{\underset{\sim}{q}}$$

Boundary conditions

Traction

$$\underline{t} = \left(\underset{\sim}{\sigma} - \nabla \cdot \underset{\sim}{\tau} + \dot{\underset{\sim}{q}} \right) \underline{n} + \nabla^S \cdot \left(\underset{\sim}{\tau} \underline{n} \right)$$



Overview of the strain gradient model

Elastic energy

$$\frac{1}{2} \left(\underset{\sim}{\sigma} : \underset{\sim}{\varepsilon} \right) + \frac{1}{2} \left(\underset{\sim}{\tau} : \nabla \underset{\sim}{\varepsilon} \right)$$

Labels: Stress tensor ($\underset{\sim}{\sigma}$), Strain tensor ($\underset{\sim}{\varepsilon}$), Hyper-Stress tensor ($\underset{\sim}{\tau}$), Gradient of strain tensor ($\nabla \underset{\sim}{\varepsilon}$)

Kinetic energy

$$\frac{1}{2} \left(\underline{\underline{p}} \cdot \underline{\underline{\dot{u}}} \right) + \frac{1}{2} \left(\underset{\sim}{q} : \nabla \underline{\underline{\dot{u}}} \right)$$

Labels: Momentum ($\underline{\underline{p}}$), Velocity ($\underline{\underline{\dot{u}}}$), Hyper momentum ($\underset{\sim}{q}$), Gradient of velocity ($\nabla \underline{\underline{\dot{u}}}$)

Balance equation

$$\nabla \cdot \left(\underset{\sim}{\sigma} - \nabla \cdot \underset{\sim}{\tau} \right) = \underline{\underline{\dot{p}}} - \nabla \cdot \underset{\sim}{\dot{q}}$$

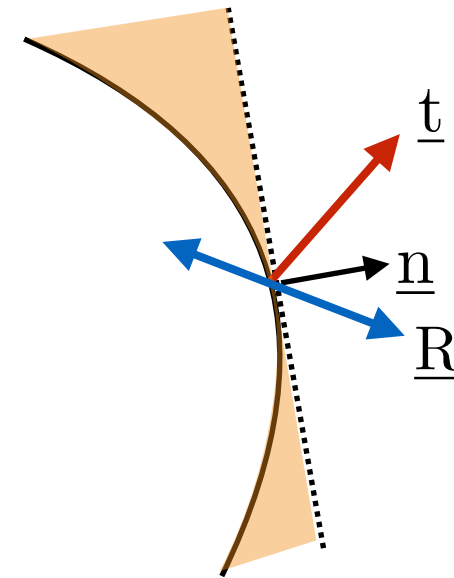
Boundary conditions

Traction

$$\underline{\underline{t}} = \left(\underset{\sim}{\sigma} - \nabla \cdot \underset{\sim}{\tau} + \underset{\sim}{\dot{q}} \right) \underline{\underline{n}} + \nabla^S \cdot \left(\underset{\sim}{\tau} \underline{\underline{n}} \right)$$

Hyper traction

$$\underline{\underline{R}} = \left(\underset{\sim}{\tau} \underline{\underline{n}} \right) \underline{\underline{n}}$$



Overview of the strain gradient model

Elastic energy

$$\frac{1}{2} \left(\underline{\underline{\sigma}} : \underline{\underline{\varepsilon}} \right) + \frac{1}{2} \left(\underline{\underline{\tau}} : \nabla \underline{\underline{\varepsilon}} \right)$$

Labels: Stress tensor ($\underline{\underline{\sigma}}$), Strain tensor ($\underline{\underline{\varepsilon}}$), Hyper-Stress tensor ($\underline{\underline{\tau}}$), Gradient of strain tensor ($\nabla \underline{\underline{\varepsilon}}$)

Kinetic energy

$$\frac{1}{2} \left(\underline{\underline{p}} \cdot \underline{\dot{\mathbf{u}}} \right) + \frac{1}{2} \left(\underline{\underline{q}} : \nabla \underline{\dot{\mathbf{u}}} \right)$$

Labels: Momentum ($\underline{\underline{p}}$), Velocity ($\underline{\dot{\mathbf{u}}}$), Hyper momentum ($\underline{\underline{q}}$), Gradient of velocity ($\nabla \underline{\dot{\mathbf{u}}}$)

Balance equation

$$\nabla \cdot \left(\underline{\underline{\sigma}} - \nabla \cdot \underline{\underline{\tau}} \right) = \underline{\dot{\mathbf{p}}} - \nabla \cdot \underline{\underline{\dot{\mathbf{q}}}}$$

Boundary conditions

Traction

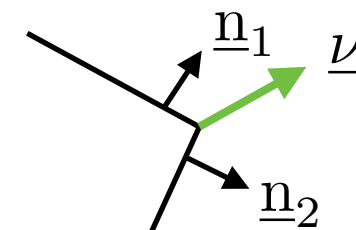
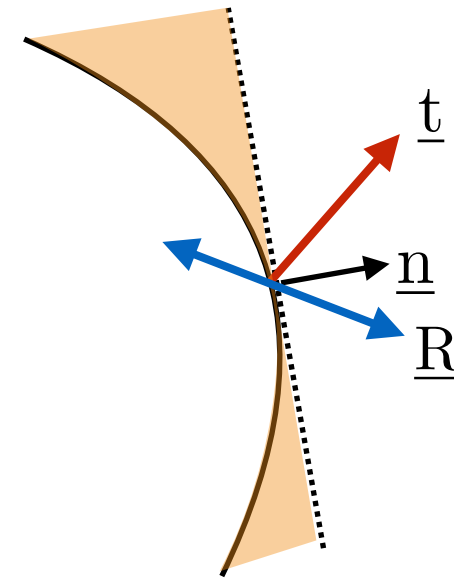
$$\underline{\underline{\mathbf{t}}} = \left(\underline{\underline{\sigma}} - \nabla \cdot \underline{\underline{\tau}} + \underline{\underline{\dot{\mathbf{q}}}} \right) \underline{\underline{\mathbf{n}}} + \nabla^S \cdot \left(\underline{\underline{\tau}} \underline{\underline{\mathbf{n}}} \right)$$

Hyper traction

$$\underline{\underline{\mathbf{R}}} = \left(\underline{\underline{\tau}} \underline{\underline{\mathbf{n}}} \right) \underline{\underline{\mathbf{n}}}$$

Edge (wedge) forces

$$\underline{\underline{\nu}} = \left[\left[\underline{\underline{\tau}} \underline{\underline{\mathbf{n}}}_1 \otimes \underline{\underline{\mathbf{n}}}_2 \right] \right]$$



Constitutive equations

The complete set of constitutive equations is

$$\begin{pmatrix} p \\ q \\ \sigma \\ \tau \end{pmatrix} = \begin{pmatrix} \rho I & K & 0 & 0 \\ K^T & J & 0 & 0 \\ 0 & 0 & C & M \\ 0 & 0 & M^T & A \end{pmatrix} \begin{pmatrix} \underline{v} \\ \nabla \underline{v} \\ \varepsilon \\ \eta \end{pmatrix}$$

		Symmetry classes	Dispersion	Non centrosymmetry	Chirality
macroscopic mass density	$\rho I_{(ij)}$	2	✗	✗	✗
classical elasticity	$C_{(ij)(kl)}$	8	✗	✗	✗

Constitutive equations

The complete set of constitutive equations is

$$\begin{pmatrix} p \\ q \\ \sigma \\ \tau \end{pmatrix} = \begin{pmatrix} \rho I & K & 0 & 0 \\ K^T & J & 0 & 0 \\ 0 & 0 & C & M \\ 0 & 0 & M^T & A \end{pmatrix} \begin{pmatrix} \underline{v} \\ \nabla \underline{v} \\ \varepsilon \\ \eta \end{pmatrix}$$

		Symmetry classes	Dispersion	Non centrosymmetry	Chirality
macroscopic mass density	$\rho I_{(ij)}$	2	✗	✗	✗
classical elasticity	$C_{(ij)(kl)}$	8	✗	✗	✗
second order inertia	$J_{(ij)(kl)}$	8	✓	✗	✗
second order elasticity	$A_{(ij)k(lm)n}$	17	✓	✗	✗

Constitutive equations

The complete set of constitutive equations is

$$\begin{pmatrix} p \\ q \\ \sigma \\ \tau \end{pmatrix} = \begin{pmatrix} \rho I & K & 0 & 0 \\ K^T & J & 0 & 0 \\ 0 & 0 & C & M \\ 0 & 0 & M^T & A \end{pmatrix} \begin{pmatrix} \underline{v} \\ \nabla \underline{v} \\ \varepsilon \\ \eta \end{pmatrix}$$

		Symmetry classes	Dispersion	Non centrosymmetry	Chirality
macroscopic mass density	$\rho I_{(ij)}$	2	✗	✗	✗
classical elasticity	$C_{(ij)(kl)}$	8	✗	✗	✗
second order inertia	$J_{(ij)(kl)}$	8	✓	✗	✗
second order elasticity	$A_{(ij)k(lm)n}$	17	✓	✗	✗
coupling inertia	K_{ijk}	17	✓	✓	✓
coupling elasticity	$M_{(ij)(lm)n}$	29	✓	✓	✓

Constitutive equations

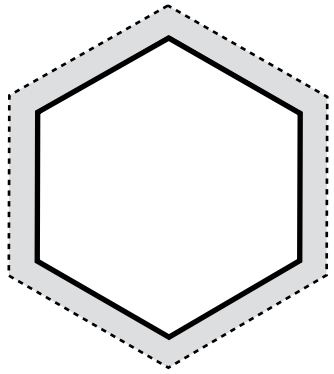
The complete set of constitutive equations is

$$\begin{pmatrix} p \\ q \\ \sigma \\ \tau \end{pmatrix} = \begin{pmatrix} \rho I & K & 0 & 0 \\ K^T & J & 0 & 0 \\ 0 & 0 & C & M \\ 0 & 0 & M^T & A \end{pmatrix} \begin{pmatrix} \underline{v} \\ \nabla \underline{v} \\ \varepsilon \\ \eta \end{pmatrix}$$

		Symmetry classes	Dispersion	Non centrosymmetry	Chirality
macroscopic mass density	$\rho I_{(ij)}$	2	✗	✗	✗
classical elasticity	$C_{(ij)(kl)}$	8	✗	✗	✗
second order inertia	$J_{(ij)(kl)}$	8	✓	✗	✗
second order elasticity	$A_{(ij)k(lm)n}$	17	✓	✗	✗
coupling inertia	K_{ijk}	17	✓	✓	✓
coupling elasticity	$M_{(ij)(lm)n}$	29	✓	✓	✓

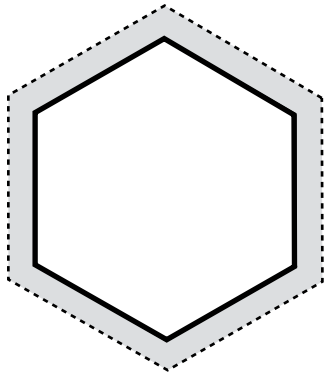
a total of 48 classes

Hexagonal honeycomb in 2D plane strain



$$\begin{pmatrix} \rho \\ \mathbf{K} \\ \mathbf{C} \\ \mathbf{M}^T \end{pmatrix} = \begin{pmatrix} \rho \mathbf{I} & \mathbf{K} & 0 & 0 \\ \mathbf{K}^T & \mathbf{J} & 0 & 0 \\ 0 & 0 & \mathbf{C} & \mathbf{M} \\ 0 & 0 & \mathbf{M}^T & \mathbf{A} \end{pmatrix} \begin{pmatrix} \mathbf{v} \\ \nabla \mathbf{v} \\ \boldsymbol{\varepsilon} \\ \boldsymbol{\eta} \end{pmatrix}$$

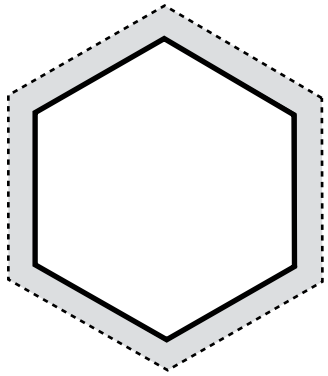
Hexagonal honeycomb in 2D plane strain



Six rotational symmetries

$$\begin{pmatrix} \rho \\ \mathbf{K} \\ \mathbf{C} \\ \mathbf{M}^T \end{pmatrix} = \begin{pmatrix} \rho \mathbf{I} & \mathbf{K} & 0 & 0 \\ \mathbf{K}^T & \mathbf{J} & 0 & 0 \\ 0 & 0 & \mathbf{C} & \mathbf{M} \\ 0 & 0 & \mathbf{M}^T & \mathbf{A} \end{pmatrix} \begin{pmatrix} \mathbf{v} \\ \nabla \mathbf{v} \\ \boldsymbol{\varepsilon} \\ \boldsymbol{\eta} \end{pmatrix}$$

Hexagonal honeycomb in 2D plane strain

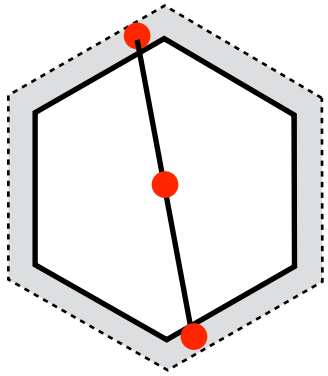


Six rotational symmetries

Six mirror planes

$$\begin{pmatrix} \rho \\ \mathbf{K} \\ \mathbf{C} \\ \mathbf{M}^T \end{pmatrix} = \begin{pmatrix} \rho \mathbf{I} & \mathbf{K} & 0 & 0 \\ \mathbf{K}^T & \mathbf{J} & 0 & 0 \\ 0 & 0 & \mathbf{C} & \mathbf{M} \\ 0 & 0 & \mathbf{M}^T & \mathbf{A} \end{pmatrix} \begin{pmatrix} \mathbf{v} \\ \nabla \mathbf{v} \\ \boldsymbol{\varepsilon} \\ \boldsymbol{\eta} \end{pmatrix}$$

Hexagonal honeycomb in 2D plane strain



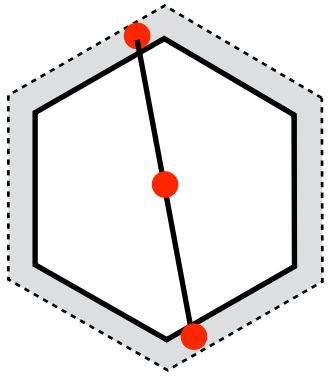
Six rotational symmetries

Six mirror planes

A center of symmetry

$$\begin{pmatrix} \rho \\ \alpha \\ \beta \\ \gamma \\ \delta \\ \epsilon \end{pmatrix} = \begin{pmatrix} \rho I & \cancel{K} & 0 & 0 \\ \cancel{K} & J & 0 & 0 \\ 0 & 0 & C & \cancel{A} \\ 0 & 0 & \cancel{A} & A \end{pmatrix} \begin{pmatrix} v \\ \nabla v \\ \epsilon \\ \eta \end{pmatrix}$$

Hexagonal honeycomb in 2D plane strain



Six rotational symmetries

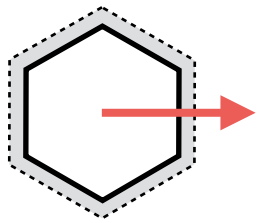
Six mirror planes

A center of symmetry

$$\begin{pmatrix} \rho \\ \mu \\ \alpha \\ \beta \\ \gamma \\ \delta \end{pmatrix} = \begin{pmatrix} \rho I & \times & 0 & 0 \\ \times & J & 0 & 0 \\ 0 & 0 & C & \times \\ 0 & 0 & \times & A \end{pmatrix} \begin{pmatrix} v \\ \nabla v \\ \varepsilon \\ \eta \end{pmatrix}$$

The generalised Christoffel equation for the directions $\theta = 0^\circ$ and $\theta = 30^\circ$ gives the following phase velocities

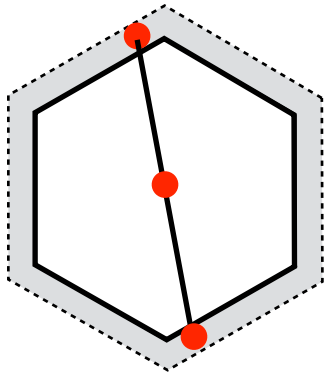
$$\theta = 0^\circ$$



$$v_p(k) = \sqrt{\frac{c_P + (a_P + a_D)k^2}{\rho + J_P k^2}}$$

$$v_s(k) = \sqrt{\frac{c_S + a_S k^2}{\rho + J_S k^2}}$$

Hexagonal honeycomb in 2D plane strain



Six rotational symmetries

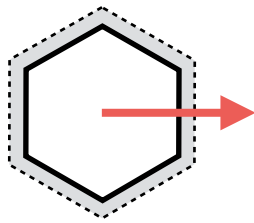
Six mirror planes

A center of symmetry

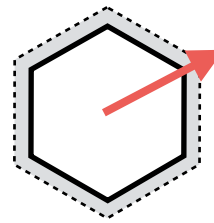
$$\begin{pmatrix} \rho \\ \rho I \\ K \\ 0 \\ 0 \end{pmatrix} = \begin{pmatrix} \rho I & \times & 0 & 0 \\ \times & J & 0 & 0 \\ 0 & 0 & C & \times \\ 0 & 0 & \times & A \end{pmatrix} \begin{pmatrix} v \\ \nabla v \\ \varepsilon \\ \eta \end{pmatrix}$$

The generalised Christoffel equation for the directions $\theta = 0^\circ$ and $\theta = 30^\circ$ gives the following phase velocities

$\theta = 0^\circ$



$\theta = 30^\circ$



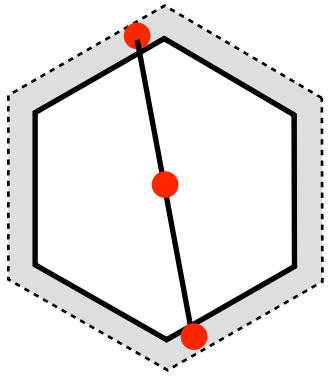
$$v_p(k) = \sqrt{\frac{c_P + (a_P + a_D)k^2}{\rho + J_P k^2}}$$

$$v_p(k) = \sqrt{\frac{c_P + a_P k^2}{\rho + J_P k^2}}$$

$$v_s(k) = \sqrt{\frac{c_S + a_S k^2}{\rho + J_S k^2}}$$

$$v_s(k) = \sqrt{\frac{c_S + (a_S + a_D)k^2}{\rho + J_S k^2}}$$

Hexagonal honeycomb in 2D plane strain



Six rotational symmetries

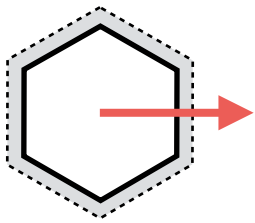
Six mirror planes

A center of symmetry

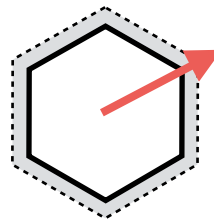
$$\begin{pmatrix} p \\ \rho \\ \alpha \\ \beta \\ \gamma \\ \tau \end{pmatrix} = \begin{pmatrix} \rho I & \times & 0 & 0 \\ \times & J & 0 & 0 \\ 0 & 0 & C & \times \\ 0 & 0 & \times & A \end{pmatrix} \begin{pmatrix} v \\ \nabla v \\ \varepsilon \\ \eta \end{pmatrix}$$

The generalised Christoffel equation for the directions $\theta = 0^\circ$ and $\theta = 30^\circ$ gives the following phase velocities

$\theta = 0^\circ$



$\theta = 30^\circ$



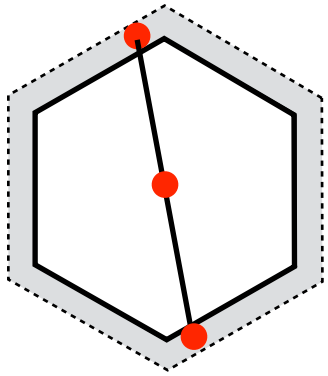
$$v_p(k) = \sqrt{\frac{c_P + (a_P + a_D)k^2}{\rho + J_P k^2}}$$

$$v_p(k) = \sqrt{\frac{c_P + a_P k^2}{\rho + J_P k^2}}$$

$$v_s(k) = \sqrt{\frac{c_S + a_S k^2}{\rho + J_S k^2}}$$

$$v_s(k) = \sqrt{\frac{c_S + (a_S + a_D)k^2}{\rho + J_S k^2}}$$

Hexagonal honeycomb in 2D plane strain



Six rotational symmetries

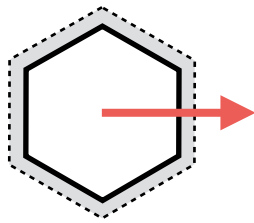
Six mirror planes

A center of symmetry

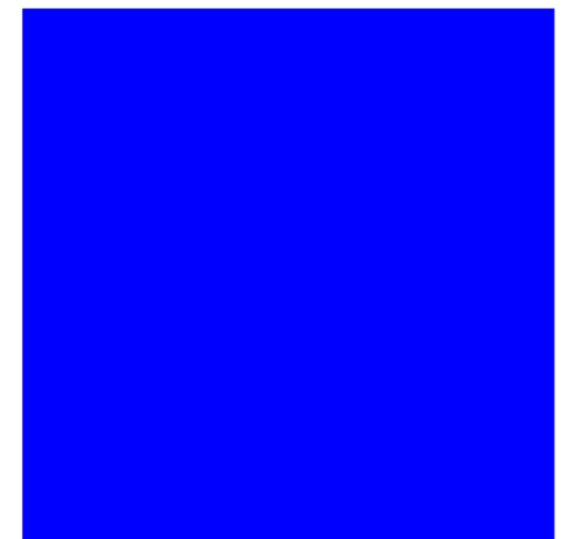
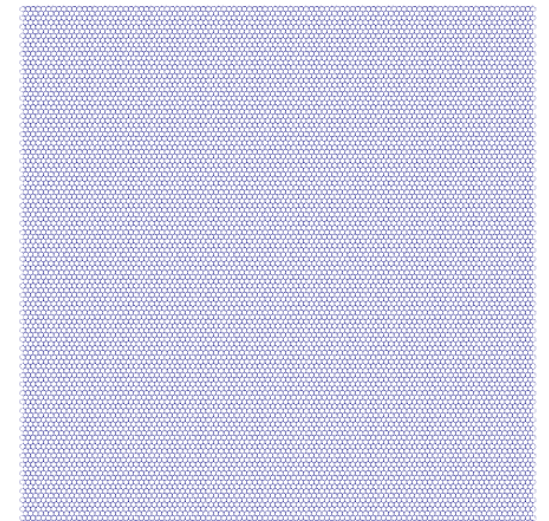
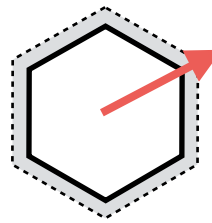
$$\begin{pmatrix} p \\ \rho \\ \sigma \\ \tau \\ \omega \\ \Omega \end{pmatrix} = \begin{pmatrix} \rho I & \times & 0 & 0 \\ \times & J & 0 & 0 \\ 0 & 0 & C & \times \\ 0 & 0 & \times & A \end{pmatrix} \begin{pmatrix} v \\ \nabla v \\ \varepsilon \\ \eta \end{pmatrix}$$

The generalised Christoffel equation for the directions $\theta = 0^\circ$ and $\theta = 30^\circ$ gives the following phase velocities

$\theta = 0^\circ$



$\theta = 30^\circ$



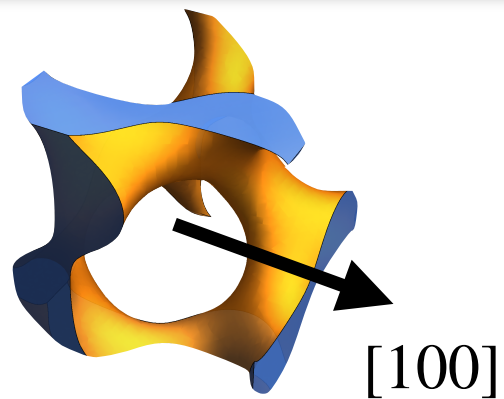
$$v_p(k) = \sqrt{\frac{c_P + (a_P + a_D)k^2}{\rho + J_P k^2}}$$

$$v_p(k) = \sqrt{\frac{c_P + a_P k^2}{\rho + J_P k^2}}$$

$$v_s(k) = \sqrt{\frac{c_S + a_S k^2}{\rho + J_S k^2}}$$

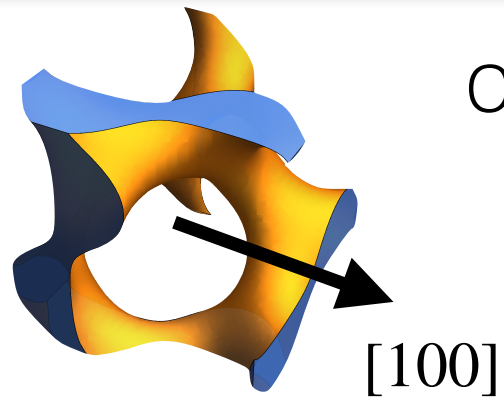
$$v_s(k) = \sqrt{\frac{c_S + (a_S + a_D)k^2}{\rho + J_S k^2}}$$

Phase velocities and polarisations



$$\begin{pmatrix} p \\ q \\ r \end{pmatrix} = \begin{pmatrix} \rho I & K & 0 & 0 \\ K^T & J & 0 & 0 \\ 0 & 0 & C & M \\ 0 & 0 & M^T & A \end{pmatrix} \begin{pmatrix} v \\ \nabla v \\ \varepsilon \\ \eta \end{pmatrix}$$

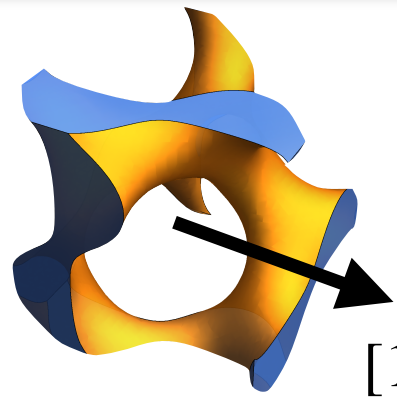
Phase velocities and polarisations



Cubic symmetry

$$\begin{pmatrix} p \\ q \\ r \end{pmatrix} = \begin{pmatrix} \rho I & K & 0 & 0 \\ K^T & J & 0 & 0 \\ 0 & 0 & C & M \\ 0 & 0 & M^T & A \end{pmatrix} \begin{pmatrix} v \\ \nabla v \\ \varepsilon \\ \eta \end{pmatrix}$$

Phase velocities and polarisations



Cubic symmetry

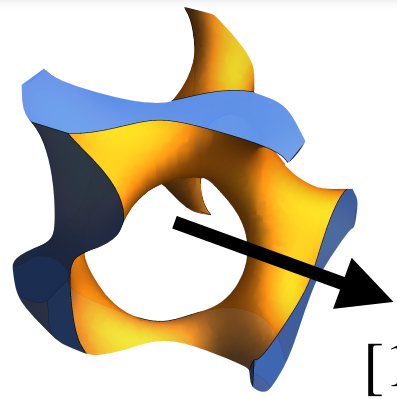
Chiral

(No center of symmetry)

[100]

$$\begin{pmatrix} p \\ q \\ \rho \\ \tau \end{pmatrix} = \begin{pmatrix} \rho I & K & 0 & 0 \\ K^T & J & 0 & 0 \\ 0 & 0 & C & M \\ 0 & 0 & M^T & A \end{pmatrix} \begin{pmatrix} v \\ \nabla v \\ \varepsilon \\ \eta \end{pmatrix}$$

Phase velocities and polarisations



Cubic symmetry

Chiral

(No center of symmetry)

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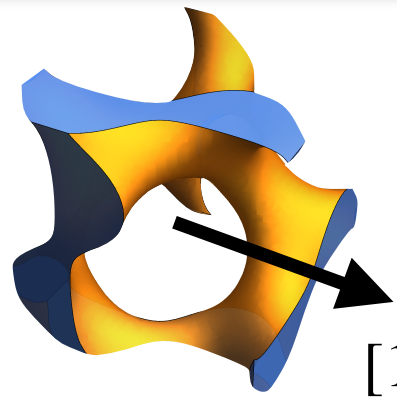
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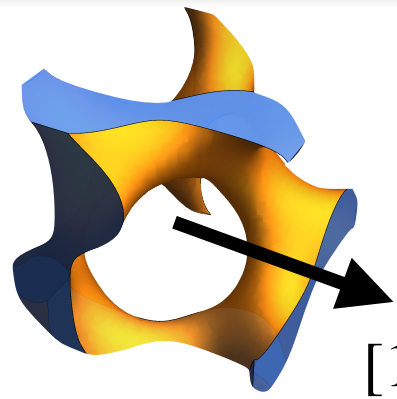
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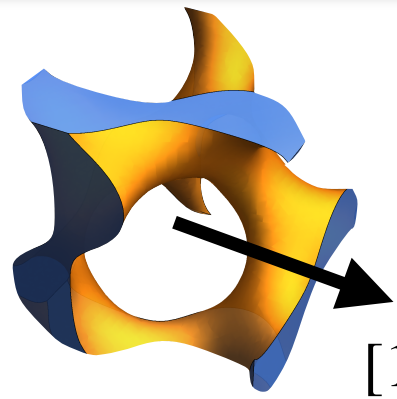
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Phase velocities and polarisations



Cubic symmetry

Chiral

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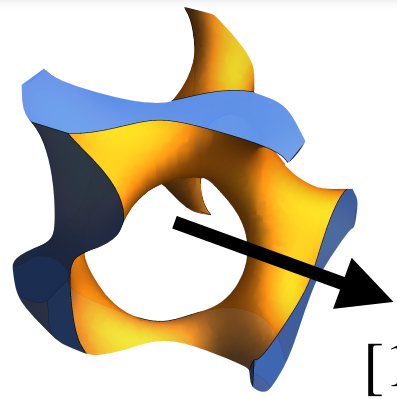
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Phase velocities and polarisations



Cubic symmetry
Chiral
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and complex polarisations

$$\underline{u}_1 = (0, -i, 1)$$

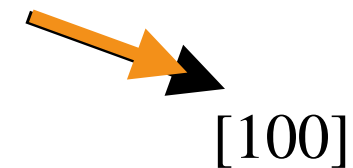
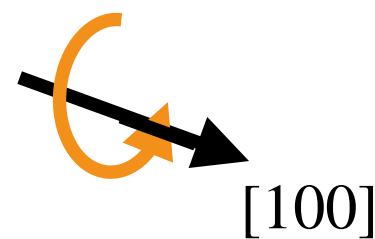
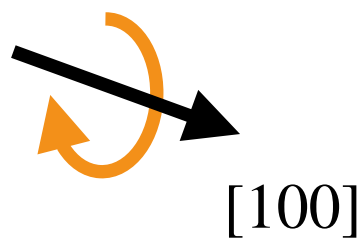
$$\underline{u}_2 = (0, i, 1)$$

$$\underline{u}_3 = (0, 0, 1)$$

Circular LH

Circular RH

Linear



$$\underline{u}_1 \cdot \underline{u}_1 = 0$$

$$\underline{u}_2 \cdot \underline{u}_2 = 0$$

$$\underline{u}_3^R \times \underline{u}_3^I = \underline{0}$$

$$\begin{bmatrix} u_2^R & u_2^I & n \end{bmatrix} > 0$$

$$\begin{bmatrix} u_2^R & u_2^I & n \end{bmatrix} < 0$$

Conclusions and perspectives

Main results

- Generalised continua are an effective tool to study wave propagation in architected material
- Results from metamaterials can be of use in biomechanics

Perspectives for biomechanical metamaterials

- Optimisation of ultrasonic properties (tailored ultrasonic signature)
- Enhanced osteointegration monitoring
- Real time quality assessment of the microstructure (phononic properties)

Things to do next

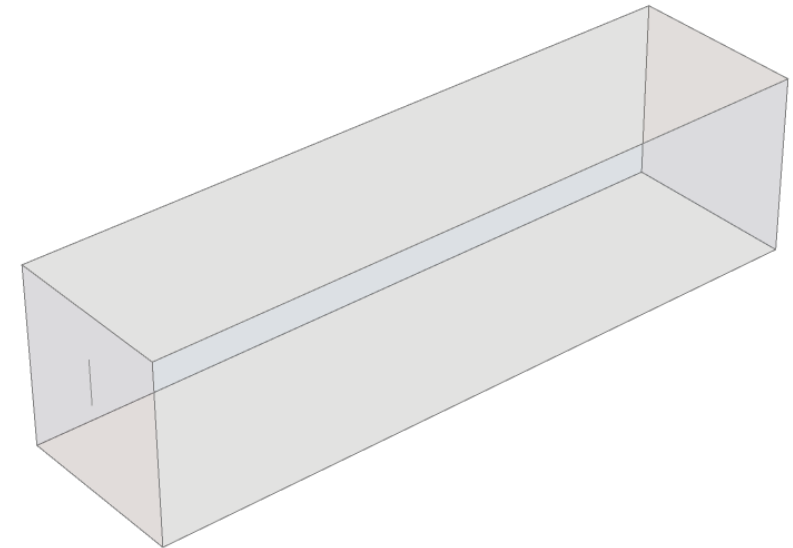
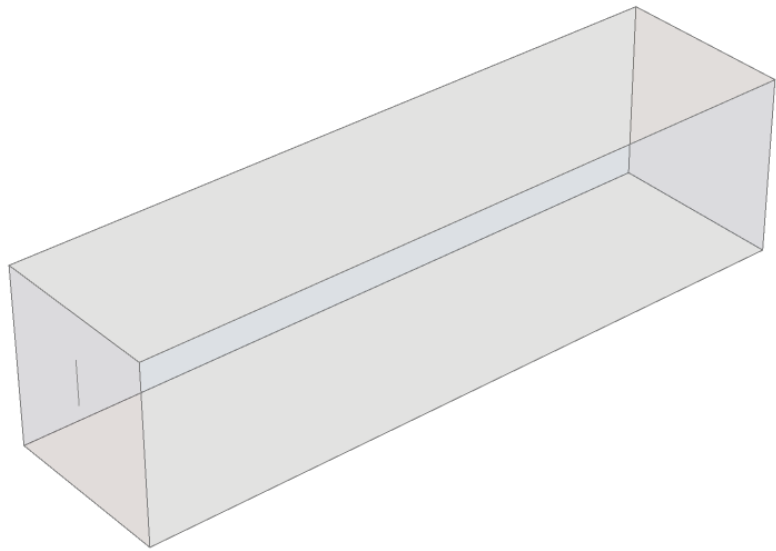
- Experimental validation (in progress)
- Reliable procedure for the estimation of the coefficients (based on guided propagation)

References

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- [2] G. Rosi and N. Auffray, “Anisotropic and dispersive wave propagation within strain-gradient framework,” *Wave Motion*, vol. 63, pp. 120–134, 2016.
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- [4] G. Rosi and N. Auffray, “Continuum modelling of frequency dependent acoustic beam focusing and steering in hexagonal lattices”, *Eur. J. Mech. A-Solids*, 2019
- [5] G. Rosi, N. Auffray, C. Combescure (2020). On the failure of classic elasticity in predicting elastic wave propagation in gyroid lattices for very long wavelengths. *Symmetry*

Polarisation of waves

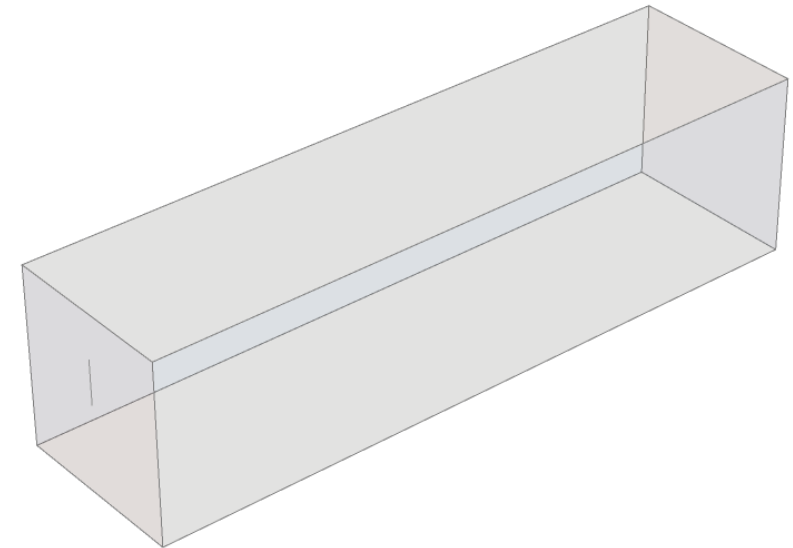
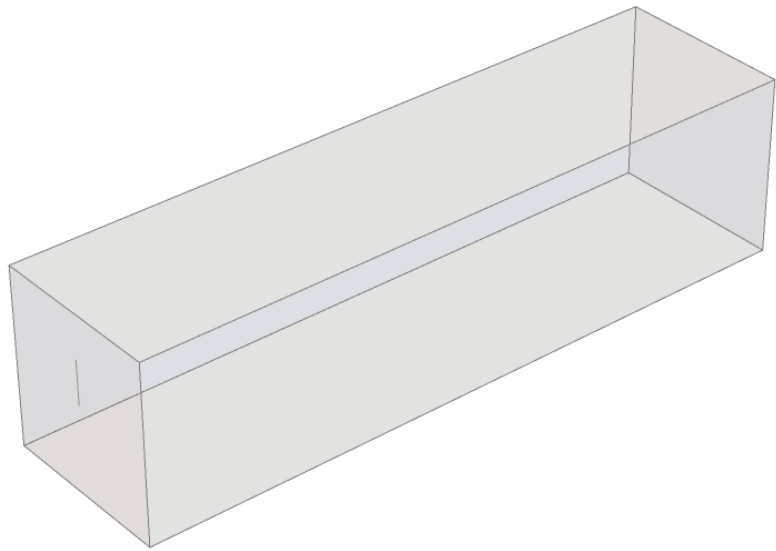
Gyroid architectures can sustain circular polarisation.



Circularly polarised waves does not propagate at the same speed

Polarisation of waves

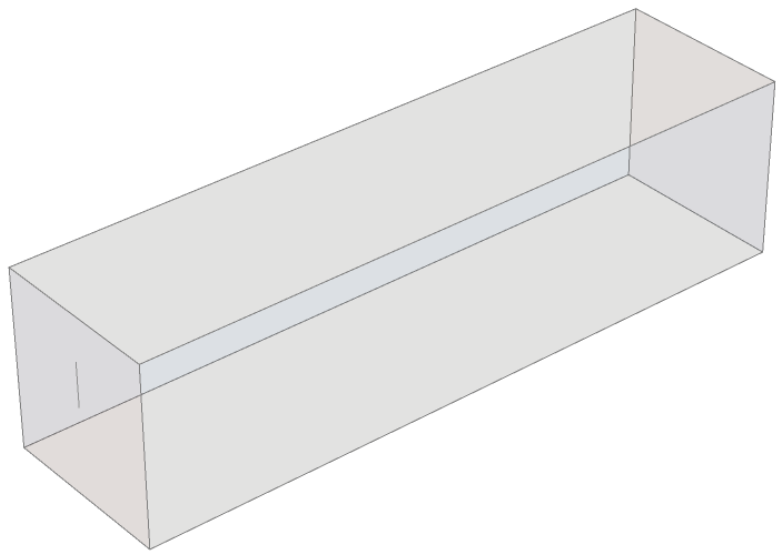
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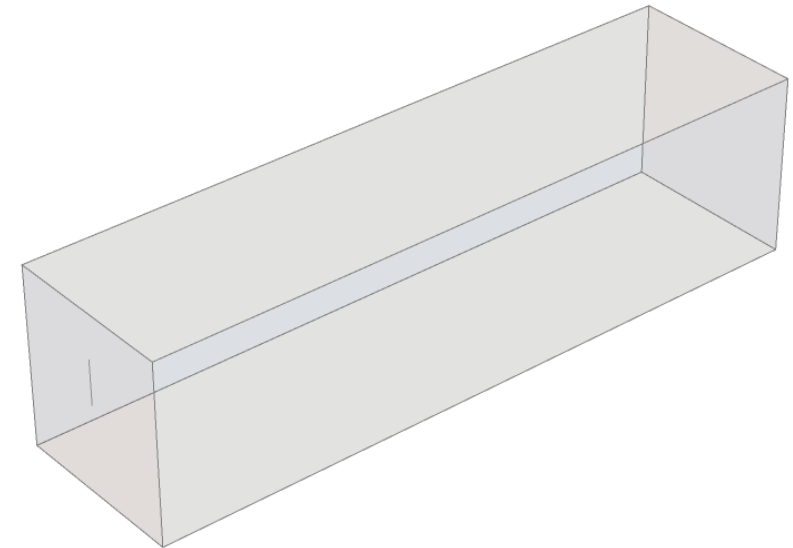
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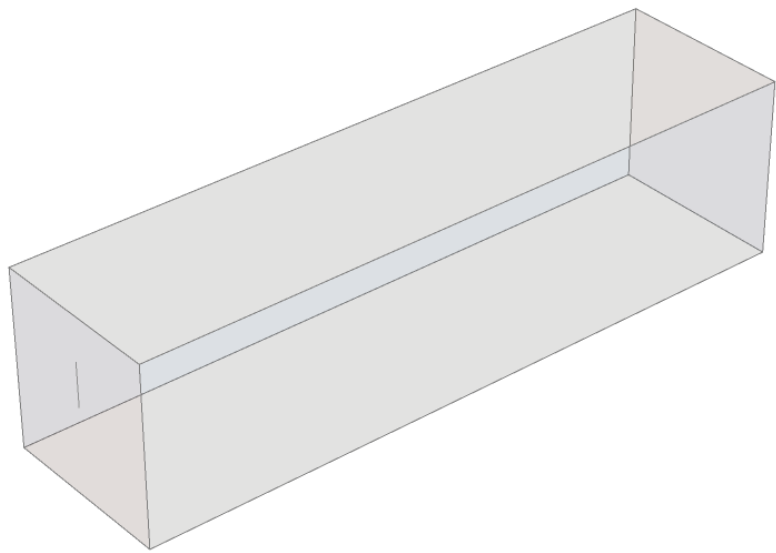
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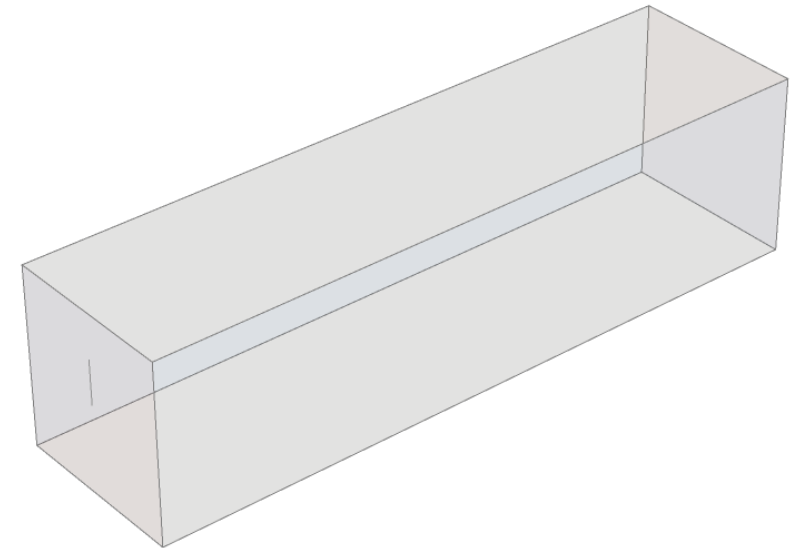
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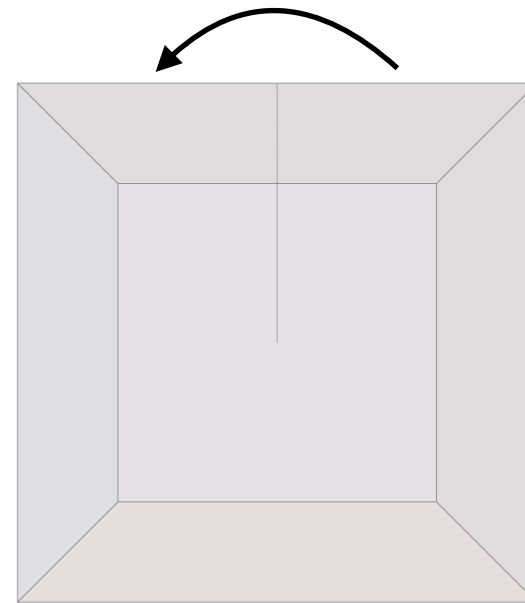
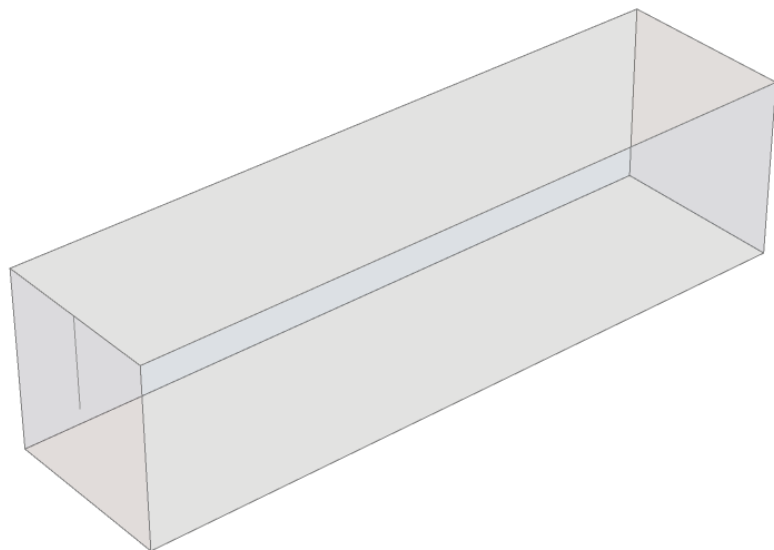
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Some additional motivations from crystallography

Neumann's principle (Curie laws)

“if a **crystal** is **invariant** with respect to certain **symmetry operations**, any of its **physical properties** must also be **invariant** with respect to the **same symmetry operations**”

or otherwise stated

“the **symmetry operations of any physical property of a crystal must include the symmetry operations of the point group of the crystal**”

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Hermann theorem of crystal physics

If we consider a **r-rank** tensor with reference to a material having a **N-fold axis of symmetry**, and **$r < N$** , then this tensor property affectively conforms to an **infinitely-fold symmetry axis parallel to the N-fold axis**.

Hermann theorem provides a sufficient condition for transverse anisotropy